EECE 360 Lecture 22



Frequency Response: Bode Diagrams

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Chapter 8.1-8.3, 8.5, 8.8

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Review: Bode Diagram

- Evaluate the gain and phase of a transfer function G(s) for $s=j\omega$
- General procedure:
 - Start a low frequencies
 - Identify break points
 - Approximate gain before and after break points
 - Approximate phase before and after break points
 - Effect is cumulative as frequency increases, for gain and phase



Outline

- Review
 - Frequency response
 - Bode diagrams for common elements
- Today
 - Sketching Bode diagrams
 - Performance requirements
 - Relationship to Root Locus
 - Gain and phase margin

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Review: Bode Diagram G(s) = K



- Log gain $20\log|G(j\omega)| = 20\log K$
- Phase

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 $\angle G(j\omega) = 0^0$



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Sketching Bode Diagrams

1. Factor transfer function

 $G(s) = \frac{K_0 \prod_i (j\omega/z_i + 1)}{(j\omega)^n \prod_j (j\omega/p_j + 1) \prod_k (1 + 2\xi_k \omega/\omega_{n,k} + (\omega/\omega_{n,k})^2)}$

- 2. Plot K₀/(jω)ⁿ
 - Gain slope *n* through K_0 at $\omega = 1$
 - Phase is -*n**90 degrees at low frequencies

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Performance specifications

- For 2nd-order systems, transient response characteristics can be estimated from Bode diagrams
- Maximum gain $M_{p\omega} = |G(\omega_r)| = \frac{1}{2\zeta\sqrt{1-\zeta^2}}$

occurs at the resonant frequency

$$\omega_r = \omega_n \sqrt{1 - 2\xi^2}$$

Also note the gain at the natural frequency is

$$\left|G(j\omega_n)\right| = \frac{1}{2\xi}$$

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Sketching Bode Diagrams

- 3. Plot remaining terms in ascending break point frequencies.
 - Extend $K_0/(j\omega)^n$ slope until first freq. break point.
 - Change gain slope by ±20dB/decade) for each zero/pole
 - Change phase by ±90 degrees for each zero/pole
- 4. Identify known points (gain at break points and resonant frequencies, phase at break points)
- 5. Smooth linear approximation in gain and phase.
- See example in Lecture 21

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Performance specifications

- Bandwidth of 1st and 2nd order systems is a good measure of the speed of the transient response
- In first-order systems, the breakpoint frequency is the bandwidth

$$\omega_B = \frac{1}{\tau}$$

In second-order systems,

$$\frac{\omega_B}{\omega_n} = -1.19\zeta + 1.85 \text{ for } 0.3 \le \zeta \le 0.8$$

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Performance specifications

- Steady-state error can be determined from a Bode diagram
- At low frequencies

$$G(j\omega) \approx \frac{K_0}{(j\omega)^n}$$

- Evaluate the gain K_0 at $\omega = 1$
 - For type 0 systems, K₀=K_p
 - For type 1 systems, $K_0 = K_v$
 - For type 2 systems, $K_0 = K_a$

Performance specifications





Relationship to Root Locus

- In Bode plots, we are interested in $s = j\omega$
- In root locus plots, we are interested in s = σ+jω such that 1+KG(s)=0 (assuming unity feedback).
- For systems whose root locus intersects the imaginary axis:
 - The crossover frequency can be identified on the Bode plots where the phase is -180 degrees.
 - Recall that *s* which satisfy the characteristic equation have a phase

$$\angle G(s) = \frac{-1}{K} = 180 \pm 360n, \quad n \in \{0, 1, 2, ...\}$$

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-20

-90

-270 0.1 Phase margin

0.5

1

ω

2

5

10

20

 $\phi(\omega) = -180$

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- The **phase margin** is the amount of phase by which G(jω) exceeds -180 degrees when |KG(jω)|=1
- These are easily measured on Bode diagrams.

Derivations and formal definitions will be provided when we investigate the Nyquist criterion (next week).

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Gain Margin

- Factor by which the gain can be increased in order to achieve marginal stability
- Measured where the phase is -180 degrees.

Gain Margin = $\frac{1}{|KG(j\omega_{180})|}$, $\omega_{180} = \arg(\angle G(j\omega) = -180)$ $M_G = -20\log G(j\omega_{180}) \,\mathrm{dB}$

- Can be stated as absolute value or in dB
- For stability, M_G > 0 dB
- Reasonable values are often 2-5, or between 6dB-14dB on a Bode diagram

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• Consider the open-loop system

$$G(s) = \frac{{\omega_n}^2}{s(s+2\zeta\omega_n)}$$

 With unity feedback, this results in a standard 2nd order system

$$\frac{G(s)}{1+G(s)} = \frac{1}{1+2\zeta/\omega_n s + (s/\omega_n)^2}$$

• with phase margin

$$M_{\phi} = 180^{\circ} - 90^{\circ} - \tan^{-1} \left(\frac{\omega_c}{2\xi \omega_n} \right)$$
$$= \tan^{-1} \left(2\xi \left(\frac{1}{(4\xi^4 + 1)^{1/2} - 2\xi^2} \right)^1 \right)$$

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Phase Margin

 The phase margin is the difference between -180 degrees and the phase of the system at the crossover frequency

Phase Margin = $M_{\phi} = 180^{\circ} + \arg(\angle G(j\omega_c))$

- For stability, $M_{\phi} > 0$
- Reasonable values are in the range 30°-60°
- **What about systems with multiple crossings?
- **Need to be very careful in analyzing stability through M_G and M_o on Bode plots. (e.g., what about systems which require a minimum gain for stability?)

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Phase Margin

• This can be linearly approximated by $\zeta = 0.01 M_{\phi}$



