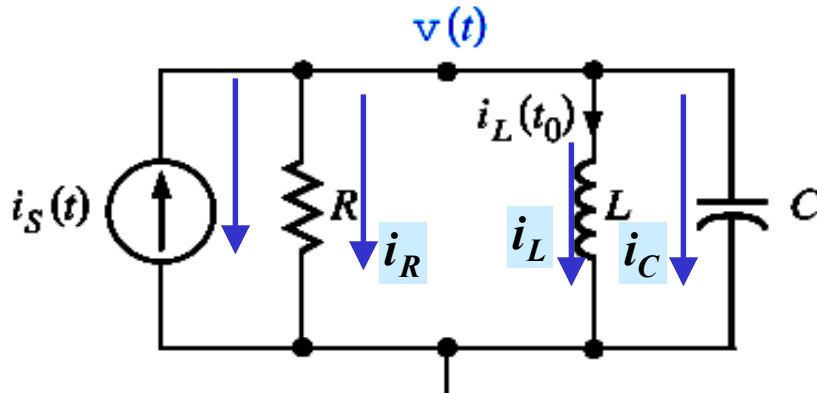


SECOND-ORDER CIRCUITS

THE BASIC CIRCUIT EQUATION



Single Node-pair: Use KCL

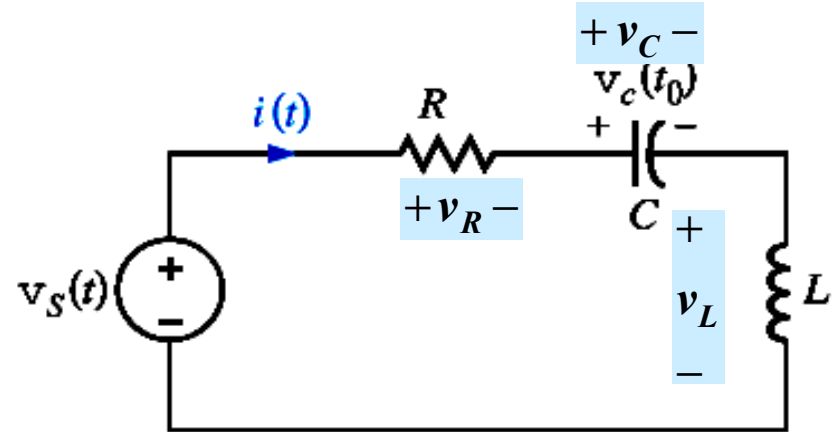
$$-i_S + i_R + i_L + i_C = 0$$

$$i_R = \frac{v(t)}{R}; \quad i_L = \frac{1}{L} \int_{t_0}^t v(x) dx + i_L(t_0); \quad i_C = C \frac{dv}{dt}(t)$$

$$\frac{v}{R} + \frac{1}{L} \int_{t_0}^t v(x) dx + i_L(t_0) + C \frac{dv}{dt}(t) = i_S$$

Differentiating

$$C \frac{d^2 v}{dt^2} + \frac{1}{R} \frac{dv}{dt} + \frac{v}{L} = \frac{di_S}{dt}$$



Single Loop: Use KVL

$$-v_S + v_R + v_C + v_L = 0$$

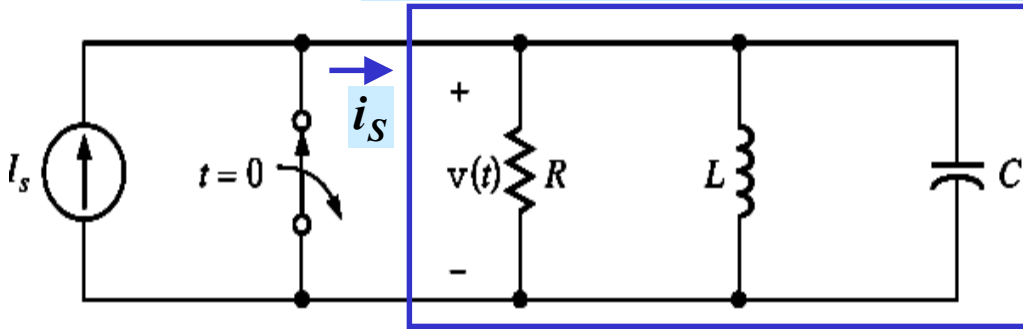
$$v_R = Ri; \quad v_C = \frac{1}{C} \int_{t_0}^t i(x) dx + v_C(t_0); \quad v_L = L \frac{di}{dt}(t)$$

$$Ri + \frac{1}{C} \int_{t_0}^t i(x) dx + v_C(t_0) + L \frac{di}{dt}(t) = v_S$$

$$L \frac{d^2 i}{dt^2} + R \frac{di}{dt} + \frac{i}{C} = \frac{dv_S}{dt}$$

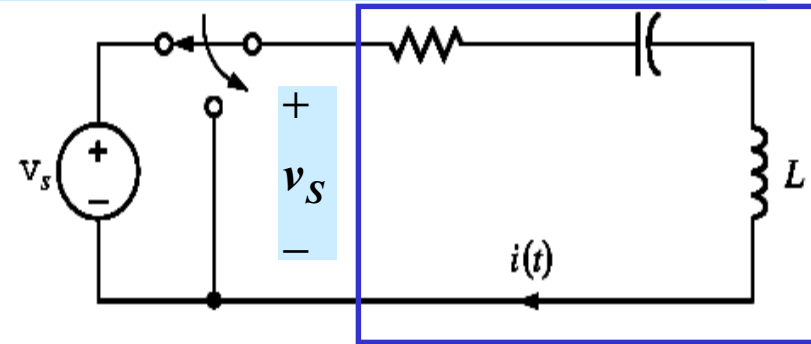


WRITE THE DIFFERENTIAL EQUATION FOR $v(t), i(t)$, RESPECTIVELY



$$i_S(t) = \begin{cases} 0 & t < 0 \\ I_S & t > 0 \end{cases}$$

$$\frac{di_S}{dt}(t) = 0; t > 0$$



$$v_S(t) = \begin{cases} V_S & t < 0 \\ 0 & t > 0 \end{cases}$$

$$\frac{dv_S}{dt}(t) = 0; t > 0$$

MODEL FOR RLC PARALLEL

$$C \frac{d^2 v}{dt^2} + \frac{1}{R} \frac{dv}{dt} + \frac{v}{L} = \frac{di_S}{dt}$$

$$C \frac{d^2 v}{dt^2} + \frac{1}{R} \frac{dv}{dt} + \frac{v}{L} = 0$$

MODEL FOR RLC SERIES

$$L \frac{d^2 i}{dt^2} + R \frac{di}{dt} + \frac{i}{C} = \frac{dv_S}{dt}$$

$$L \frac{d^2 i}{dt^2} + R \frac{di}{dt} + \frac{i}{C} = 0$$



THE RESPONSE EQUATION

WE STUDY THE SOLUTIONS FOR THE EQUATION

$$\frac{d^2 x}{dt^2}(t) + a_1 \frac{dx}{dt}(t) + a_2 x(t) = f(t)$$

KNOWN: $x(t) = x_p(t) + x_c(t)$

x_p particular solution

x_c complementary solution

THE COMPLEMENTARY SOLUTION SATISIFES

$$\frac{d^2 x_c}{dt^2}(t) + a_1 \frac{dx_c}{dt}(t) + a_2 x_c(t) = 0$$

IF THE FORCING FUNCTION IS A CONSTANT

$$f(t) = A \Rightarrow x_p = \frac{A}{a_2} \text{ is a particular solution}$$

$$\text{PROOF: } x_p = \frac{A}{a_2} \Rightarrow \frac{dx_p}{dt} = \frac{d^2 x_p}{dt^2} = 0 \Rightarrow a_2 x_p = A$$

FOR ANY FORCING FUNCTION $f(t) = A$

$$x(t) = \frac{A}{a_2} + x_c(t)$$



THE HOMOGENEOUS EQUATION

$$\frac{d^2 x}{dt^2}(t) + a_1 \frac{dx}{dt}(t) + a_2 x(t) = 0$$

NORMALIZED FORM

$$\frac{d^2 x}{dt^2}(t) + 2\zeta\omega_n \frac{dx}{dt}(t) + \omega_n^2 x(t) = 0$$

ω_n (undamped) natural frequency

ζ damping ratio

CHARACTERISTIC EQUATION

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

$$a_2 = \omega_n^2 \Rightarrow \omega_n = \sqrt{a_2}$$

$$a_1 = 2\zeta\omega_n \Rightarrow \zeta = \frac{a_1}{2\sqrt{a_2}}$$

LEARNING BY DOING

DETERMINE THE CHARACTERISTIC EQUATION, DAMPING RATIO AND NATURAL FREQUENCY

$$4 \frac{d^2 x}{dt^2}(t) + 8 \frac{dx}{dt}(t) + 16x(t) = 0$$

COEFFICIENT OF SECOND DERIVATIVE MUST BE ONE

$$\frac{d^2 x}{dt^2}(t) + 2 \frac{dx}{dt}(t) + 4x(t) = 0$$

CHARACTERISTIC EQUATION

$$s^2 + 2s + 4 = 0$$

DAMPING RATIO, NATURAL FREQUENCY

$$\frac{d^2 x}{dt^2}(t) + 2 \frac{dx}{dt}(t) + 4x(t) = 0$$

$$2\zeta\omega_n \quad \omega_n^2 \Rightarrow \omega_n = 2$$

$$\Downarrow$$
$$\zeta = 0.5$$



ANALYSIS OF THE HOMOGENEOUS EQUATION

NORMALIZED FORM

$$\frac{d^2 x}{dt^2}(t) + 2\zeta\omega_n \frac{dx}{dt}(t) + \omega_n^2 x(t) = 0$$

$$x(t) = Ke^{st} \text{ is a solution iff } s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

Iff s is solution of the *characteristic equation*

PROOF: $\frac{dx}{dt}(t) = sKe^{st}; \frac{d^2 x}{dt^2} = s^2 Ke^{st}$

$$\frac{d^2 x}{dt^2}(t) + 2\zeta\omega_n \frac{dx}{dt}(t) + \omega_n^2 x(t) = (s^2 + 2\zeta\omega_n s + \omega_n^2)Ke^{st}$$

CHARACTERISTIC EQUATION

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

$$(s + \zeta\omega_n)^2 + (\omega_n^2 - \zeta^2\omega_n^2) = 0$$

$$s = -\zeta\omega_n \pm \sqrt{\zeta^2\omega_n^2 - \omega_n^2}$$

$$s = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

(modes of the system)

CASE 1: $\zeta > 1$ (real and distinct roots)

$$x(t) = K_1 e^{s_1 t} + K_2 e^{s_2 t}$$

CASE 2: $\zeta < 1$ (complex conjugate roots)

$$x(t) = K_1 e^{s_1 t} + K_2 e^{s_2 t}$$

$$s = -\zeta\omega_n \pm j\omega_n\sqrt{1 - \zeta^2}$$

$$x(t) \text{ real} \Rightarrow K_2 = K_1^*$$

$$s = -\sigma \pm j\omega_d$$

ω_d = damped oscillation frequency

σ = damping factor

$$x(t) = e^{-\sigma t} (A_1 \cos \omega_d t + A_2 \sin \omega_d t)$$

HINT: $e^{st} = e^{-(\zeta\omega_n \pm j\omega_d)t} = e^{-\zeta\omega_n t} e^{\mp j\omega_d t}$

$$e^{\mp j\omega_d t} = \cos \omega_d t \mp j \sin \omega_d t$$

ASSUME $K_1 = (A_1 + jA_2)/2$

$$\left. \begin{matrix} K_2 = K_1^* \\ s = -\sigma \pm j\omega_d \end{matrix} \right\} \Rightarrow x(t) = 2 \operatorname{Re} [K_1 e^{-(\sigma + j\omega_d)t}]$$

CASE 3: $\zeta = 1$ (real and equal roots)

$$s = -\zeta\omega_n$$

$$x(t) = (B_1 + B_2 t) e^{-\zeta\omega_n t}$$

HINT: te^{st} is solution iff

$$(s^2 + 2\zeta\omega_n s + \omega_n^2 = 0) \text{ AND } (2s + 2\zeta\omega_n = 0)$$



LEARNING EXTENSIONS

DETERMINE THE GENERAL FORM OF THE SOLUTION

$$\frac{d^2 x}{dt^2}(t) + 4 \frac{dx}{dt}(t) + 4x(t) = 0$$

CHARACTERISTIC EQUATION

$$s^2 + 4s + 4 = 0$$

$$\omega_n^2 = 4 \Rightarrow \omega_n = 2 \quad 2\zeta\omega_n = 4 \Rightarrow \zeta = 1$$

$$s^2 + 4s + 4 = 0 \Rightarrow (s + 2)^2 = 0$$

Roots are real and equal

this is a critically damped (case 3) system

$$x(t) = (B_1 + B_2 t)e^{st}$$

$$x(t) = (B_1 + B_2 t)e^{-2t}$$

$$4 \frac{d^2 x}{dt^2}(t) + 8 \frac{dx}{dt}(t) + 16x(t) = 0$$

Divide by coefficient of second derivative

$$\frac{d^2 x}{dt^2}(t) + 2 \frac{dx}{dt}(t) + 4x(t) = 0$$

$$\omega_n^2 = 4 \Rightarrow \omega_n = 2 \quad 2\zeta\omega_n = 2 \Rightarrow \zeta = 0.5$$

$$s^2 + 2s + 4 = (s + 1)^2 + 3 = 0 \Rightarrow s = -1 \pm j\sqrt{3}$$

Roots are complex conjugate

underdamped (case 2) system

$$\sigma = \zeta\omega_n = 1; \quad \omega_d = \omega_n \sqrt{1 - \zeta^2} = 2\sqrt{1 - 0.25} = \sqrt{3}$$

$$x(t) = e^{-\sigma t} (A_1 \cos \omega_d t + A_2 \sin \omega_d t)$$

$$x(t) = e^{-t} (A_1 \cos \sqrt{3}t + A_2 \sin \sqrt{3}t)$$

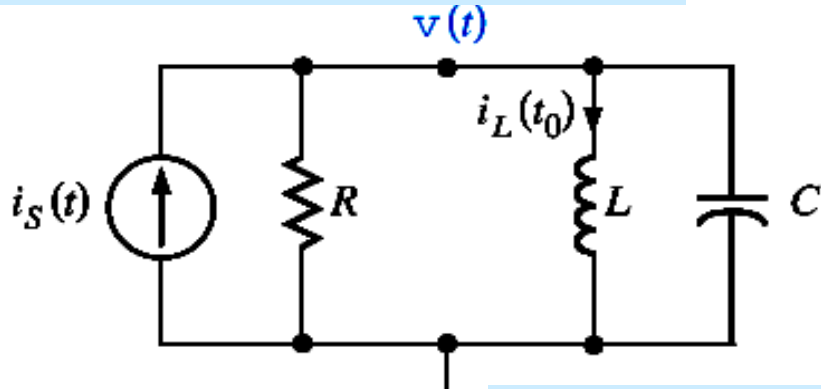
ω_d



Form of the solution

LEARNING EXTENSIONS

RLC PARALLEL CIRCUIT WITH
 $R = 1\Omega, L = 2H, C = 2F$



HOMOGENEOUS EQUATION

$$C \frac{d^2 v}{dt^2} + \frac{1}{R} \frac{dv}{dt} + \frac{v}{L} = 0$$

$$2 \frac{d^2 v}{dt^2} + \frac{dv}{dt} + \frac{v}{2} = 0$$

$$s^2 + \frac{s}{2} + \frac{1}{4} = \left(s + \frac{1}{4}\right)^2 + \frac{3}{16} = 0$$

$$\frac{d^2 v}{dt^2} + \frac{1}{2} \frac{dv}{dt} + \frac{v}{4} = 0$$

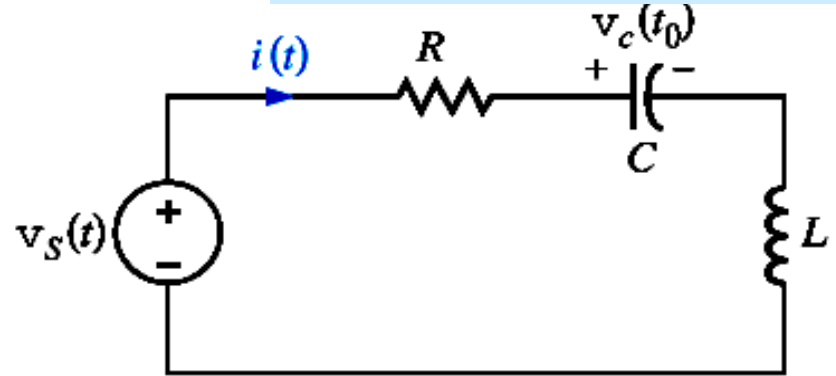
$$\omega_n = \frac{1}{2}; \zeta \omega_n = \frac{1}{4} \Rightarrow \zeta = \frac{1}{2}$$

$$\sigma = \frac{1}{4}$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2} = \frac{1}{2} \sqrt{1 - \frac{1}{4}} = \frac{\sqrt{3}}{4}$$

$$v_c(t) = e^{-\frac{t}{4}} \left(A_1 \cos \frac{\sqrt{3}}{4} t + A_2 \sin \frac{\sqrt{3}}{4} t \right)$$

RLC SERIES CIRCUIT WITH
 $R = 2\Omega; L = 1H, C = 0.5F, 1F, 2F$



Classify the responses for the given values of C

$$L \frac{d^2 i}{dt^2} + R \frac{di}{dt} + \frac{i}{C} = 0 \quad : / L \text{ \& replace values}$$

$$\frac{d^2 i}{dt^2} + 2 \frac{di}{dt} + \frac{i}{C} = 0$$

$$\omega_n = \frac{1}{\sqrt{C}}; 2\zeta\omega_n = 2 \Rightarrow \zeta = \sqrt{C}$$

- C=0.5** underdamped
- C=1.0** critically damped
- C=2.0** overdamped

$$\text{discriminant} = 4 - \frac{4}{C}$$



THE NETWORK RESPONSE

DETERMINING THE CONSTANTS

NORMALIZED FORM

$$\frac{d^2 x}{dt^2}(t) + 2\zeta\omega_n \frac{dx}{dt}(t) + \omega_n^2 x(t) = A$$

$$x(t) = \frac{A}{\omega_n^2} + K_1 e^{s_1 t} + K_2 e^{s_2 t}$$

$$x(0+) - \frac{A}{\omega_n^2} = K_1 + K_2$$

$$\frac{dx}{dt}(0+) = s_1 K_1 + s_2 K_2$$

$$x(t) = \frac{A}{\omega_n^2} + e^{-\zeta\omega_n t} (A_1 \cos \omega_d t + A_2 \sin \omega_d t)$$

$$x(0+) - \frac{A}{\omega_n^2} = A_1$$

$$\frac{dx}{dt}(0+) = -\zeta\omega_n A_1 + \omega_d A_2$$

$$x(t) = \frac{A}{\omega_n^2} + (B_1 + B_2 t) e^{-\zeta\omega_n t}$$

$$x(0+) - \frac{A}{\omega_n^2} = B_1$$

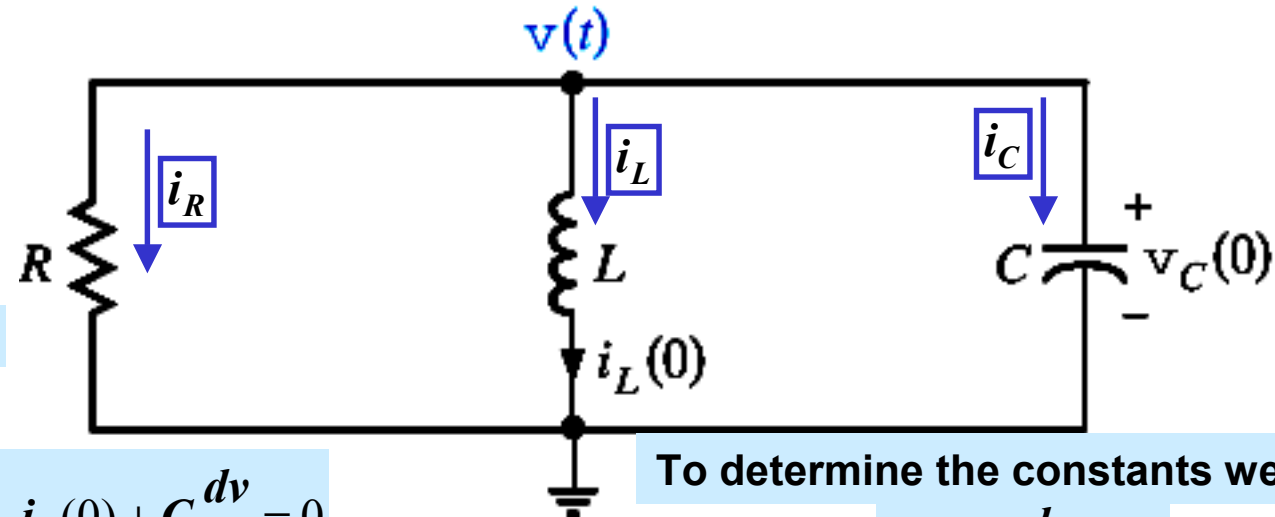
$$\frac{dx}{dt}(0+) = -\zeta\omega_n B_1 + B_2$$



LEARNING EXAMPLE

$R = 2\Omega, L = 5H, C = \frac{1}{5}F$

$i_L(0) = -1A, v_C(0) = 4V$



$i_R + i_L + i_C = 0$

$\frac{v}{R} + \frac{1}{L} \int_0^t v(x) dx + i_L(0) + C \frac{dv}{dt} = 0$

$\frac{d^2v}{dt^2} + \frac{1}{RC} \frac{dv}{dt} + \frac{1}{LC} v = 0$

**STEP 1
MODEL**

CHARACTERISTIC EQUATION

STEP 2

$s^2 + 2.5s + 1 = 0 \Rightarrow \omega_n = 1; \zeta = 1.5$

$s = \frac{-2.5 \pm \sqrt{(2.5)^2 - 4}}{2} = \frac{-2.5 \pm 1.5}{2}$

**STEP 3
ROOTS**

$v(t) = K_1 e^{-2t} + K_2 e^{-0.5t}$

**STEP 4
FORM OF
SOLUTION**

STEP 5: FIND CONSTANTS

To determine the constants we need

$v(0+); \frac{dv}{dt}(0+)$

IF NOT GIVEN FIND $v_C(0), i_L(0)$

$v(0+) = v_C(0+) = v_C(0) = 4V$

KCL AT $t = 0+$

**ANALYZE
CIRCUIT AT
t=0+**

$\frac{v_C(0+)}{R} + i_L(0+) + C \frac{dv}{dt}(0+) = 0$

$\frac{dv}{dt}(0+) = -\frac{4}{2(1/5)} - \frac{(-1)}{(1/5)} = -5$

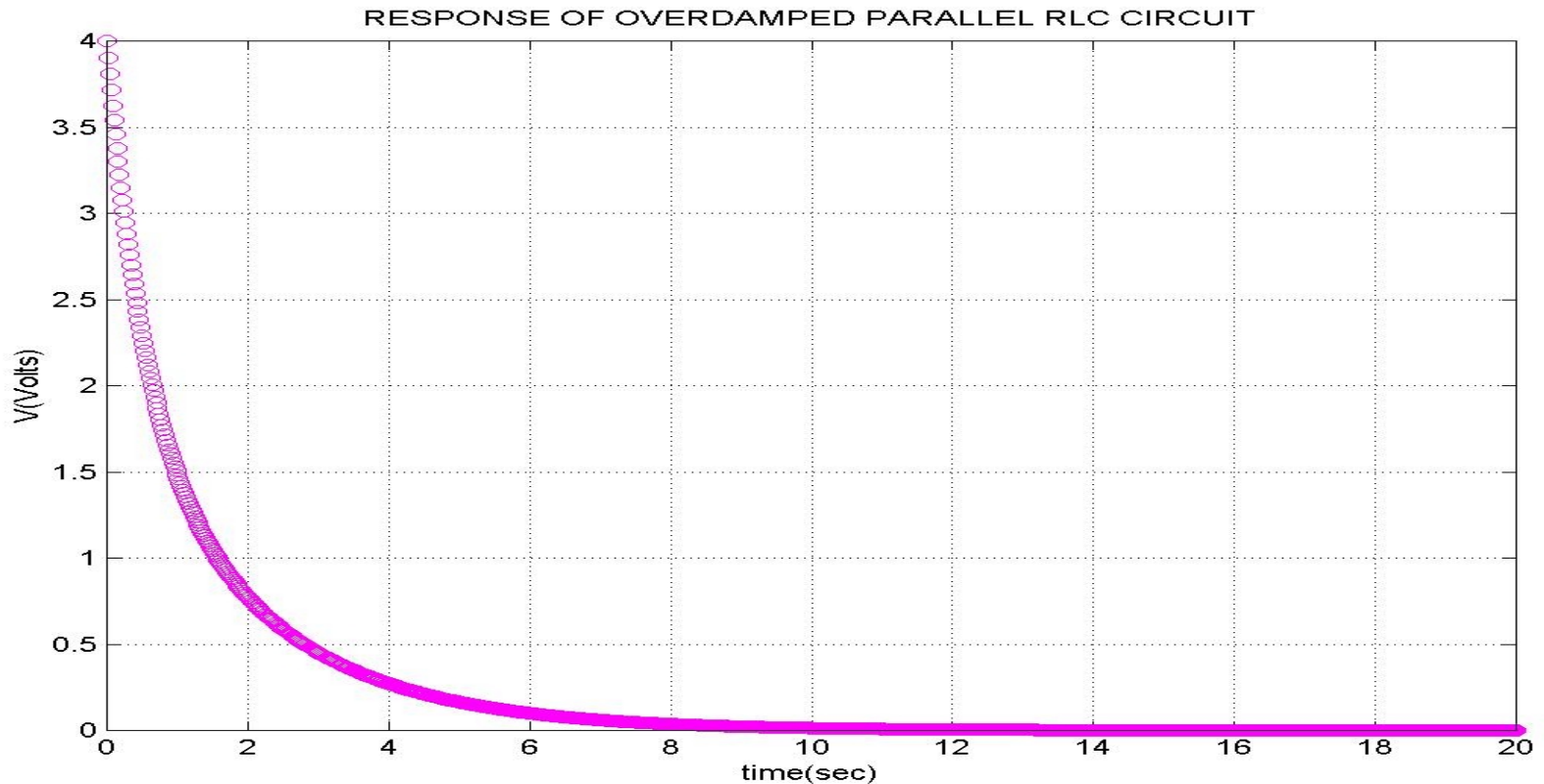
$\left. \begin{matrix} K_1 + K_2 = 4 \\ -2K_1 - 0.5K_2 = -5 \end{matrix} \right\} \Rightarrow K_1 = 2; K_2 = 2$

$v(t) = 2e^{-2t} + 2e^{-0.5t}; t > 0$



USING MATLAB TO VISUALIZE THE RESPONSE

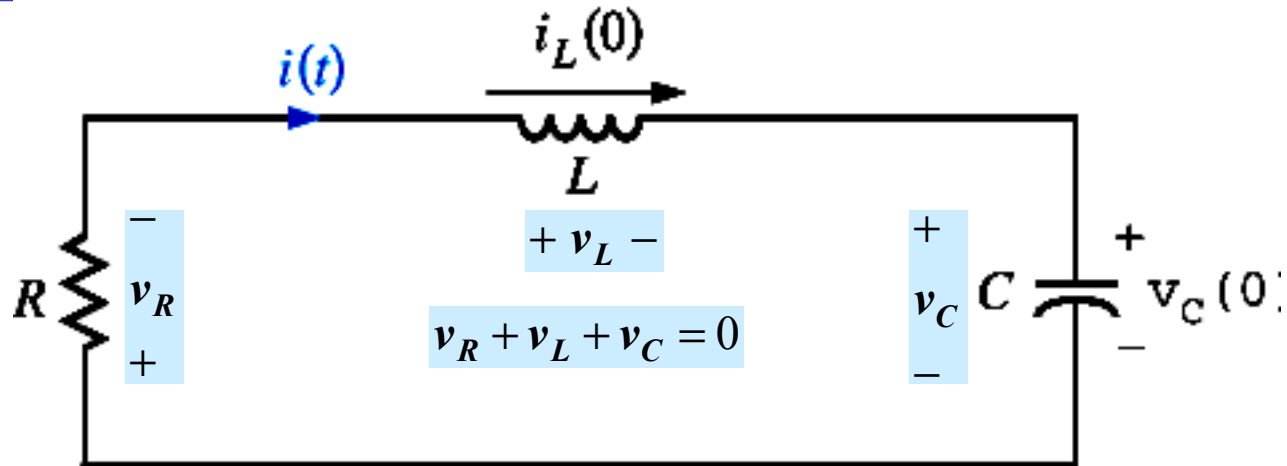
```
%script6p7.m  
%plots the response in Example 6.7  
%v(t)=2exp(-2t)+2exp(-0.5t); t>0  
t=linspace(0,20,1000);  
v=2*exp(-2*t)+2*exp(-0.5*t);  
plot(t,v,'mo'), grid, xlabel('time(sec)'), ylabel('V(Volts)')  
title('RESPONSE OF OVERDAMPED PARALLEL RLC CIRCUIT')
```



LEARNING EXAMPLE

$R = 6\Omega, L = 1H, C = 0.04F$

$i_L(0) = 4A; v_C(0) = -4V$



NO SWITCHING OR DISCONTINUITY AT $t=0$. USE $t=0$ OR $t=0+$

$Ri(t) + L \frac{di}{dt}(t) + \frac{1}{C} \int_0^t i(x) dx + v_C(0) = 0$

TO COMPUTE $\frac{di}{dt}(0+)$ $v_L(t) = L \frac{di}{dt}(t)$

$\frac{d^2i}{dt^2} + \frac{R}{L} \frac{di}{dt}(t) + \frac{1}{LC} i(t) = 0$ **model**

$L \frac{di}{dt}(0) = -Ri(0) - v_C(0) \Rightarrow \frac{di}{dt}(0+) = -20$

$\frac{d^2i}{dt^2} + 6 \frac{di}{dt}(t) + 25i(t) = 0$

$\frac{di}{dt}(t) = -3i(t) + e^{-3t}(-4A_1 \sin 4t + 4A_2 \cos 4t)$

Ch. Eq.: $s^2 + 6s + 25 = 0$
 $\omega_n^2 = 25 \Rightarrow \omega_n = 5$
 $2\zeta\omega_n = 6 \Rightarrow \zeta = 0.6$

@ $t = 0$: $-20 = -3 \times (4) + 4A_2 \Rightarrow A_2 = -2$

roots: $s = \frac{-6 \pm \sqrt{36 - 100}}{2} = -3 \pm j4$ ω_d

$i(t) = e^{-3t} (4 \cos 4t - 2 \sin 4t) [A]; t > 0$

Form: $i(t) = e^{-3t} (A_1 \cos 4t + A_2 \sin 4t)$

$v_C(t) = -Ri(t) - L \frac{di}{dt}(t) = v_C(0) + \frac{1}{C} \int_0^t i(x) dx$

$i(0) = i_L(0) = 4A \Rightarrow A_1 = 4$

$v_C(t) = e^{-3t} (-4 \cos 4t + 22 \sin 4t) [V]; t > 0$



USING MATLAB TO VISUALIZE THE RESPONSE

```
%script6p8.m
```

```
%displays the function  $i(t) = \exp(-3t) (4\cos(4t) - 2\sin(4t))$ 
```

```
% and the function  $vc(t) = \exp(-3t) (-4\cos(4t) + 22\sin(4t))$ 
```

```
% use a simple algorithm to estimate display time
```

```
tau=1/3;
```

```
tend=10*tau;
```

```
t=linspace(0,tend,350);
```

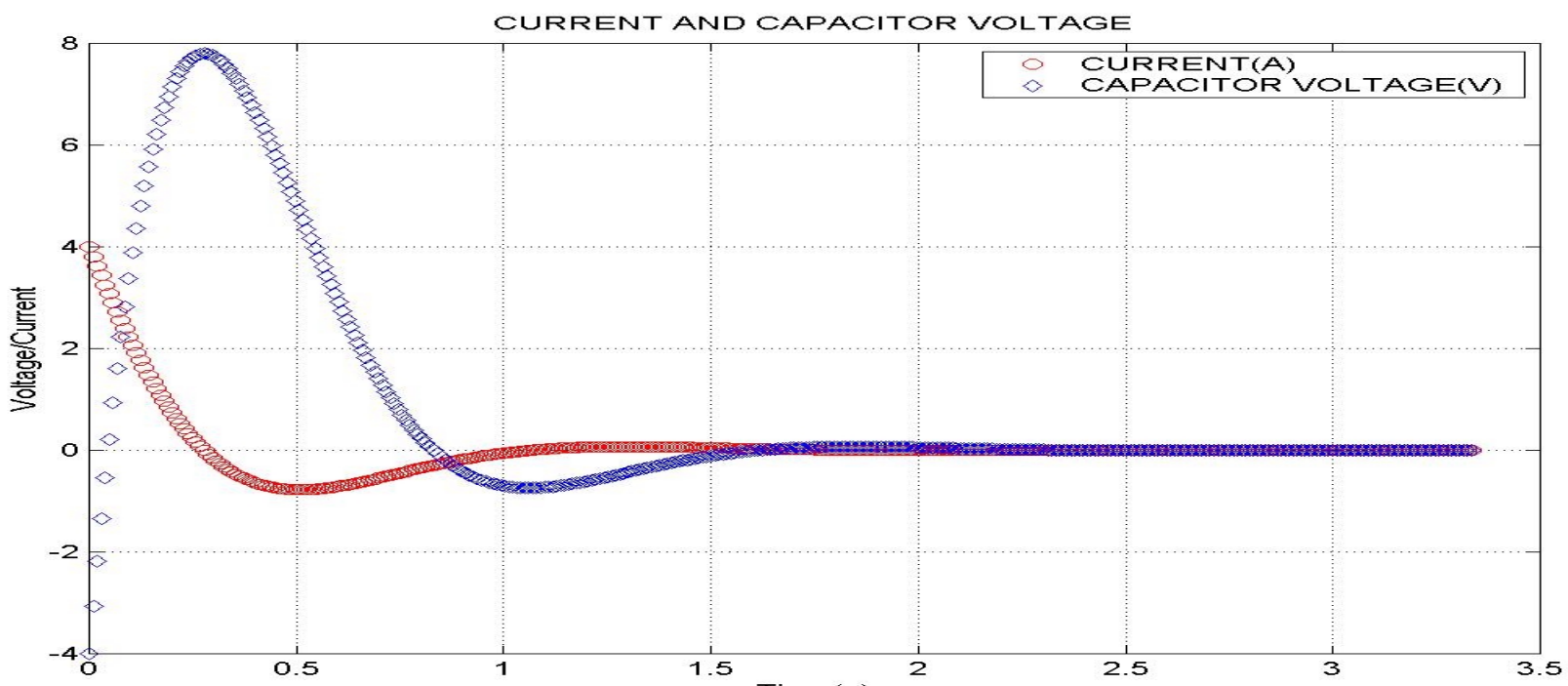
```
it=exp(-3*t).*(4*cos(4*t)-2*sin(4*t));
```

```
vc=exp(-3*t).*(-4*cos(4*t)+22*sin(4*t));
```

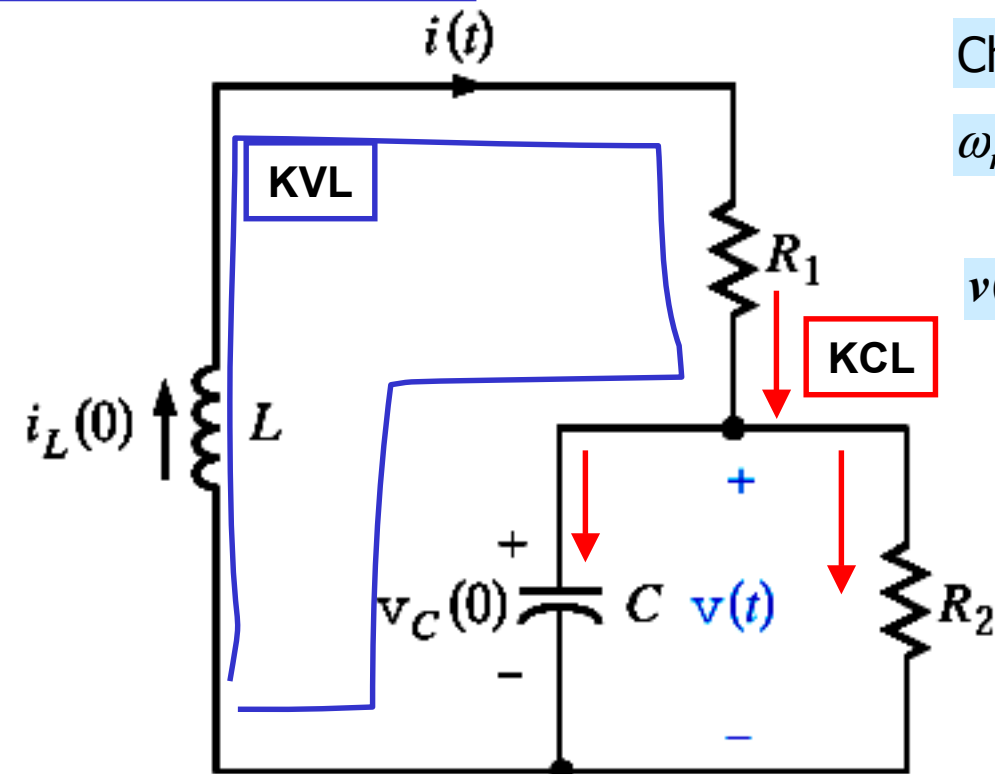
```
plot(t,it,'ro',t,vc,'bd'),grid,xlabel('Time(s)'),ylabel('Voltage/Current')
```

```
title('CURRENT AND CAPACITOR VOLTAGE')
```

```
legend('CURRENT(A)', 'CAPACITOR VOLTAGE(V)')
```



LEARNING EXAMPLE $R_1 = 10\Omega$, $R_2 = 8\Omega$, $C = 1F$, $L = 2H$ $v_C(0) = 1V$, $i_L(0) = 0.5A$



Ch. Eq.: $s^2 + 6s + 9 = 0 = (s + 3)^2$

$\omega_n = 3$, $2\zeta\omega_n = 6 \Rightarrow \zeta = 1$ $v(t) = e^{-3t}(B_1 + B_2t)$

$v(0+) = v_c(0+) = 1V$

NO SWITCHING OR DISCONTINUITY AT $t=0$. USE $t=0$ OR $t=0+$

KCL AT $t = 0+$

$i(0) = i_L(0) = \frac{v(0)}{R_2} + C \frac{dv}{dt}(0) \Rightarrow \frac{dv}{dt}(0) = 3$

$v(0) = 1 = B_1$

$\frac{dv}{dt}(0) = -3v(0) + B_2 = 3 \Rightarrow B_2 = 6$

$v(t) = e^{-3t}(1 + 6t); t > 0$

$L \frac{di}{dt}(t) + R_1 i(t) + v(t) = 0$

$i(t) = \frac{v(t)}{R_2} + C \frac{dv}{dt}(t)$

$L \left(\frac{1}{R_2} \frac{dv}{dt}(t) + C \frac{d^2v}{dt^2} \right) + R_1 \left(\frac{v(t)}{R_2} + C \frac{dv}{dt}(t) \right) + v(t) = 0$

$\frac{d^2v}{dt^2}(t) + \left(\frac{1}{R_2 C} + \frac{R_1}{L} \right) \frac{dv}{dt}(t) + \frac{R_1 + R_2}{R_2 LC} v(t) = 0$

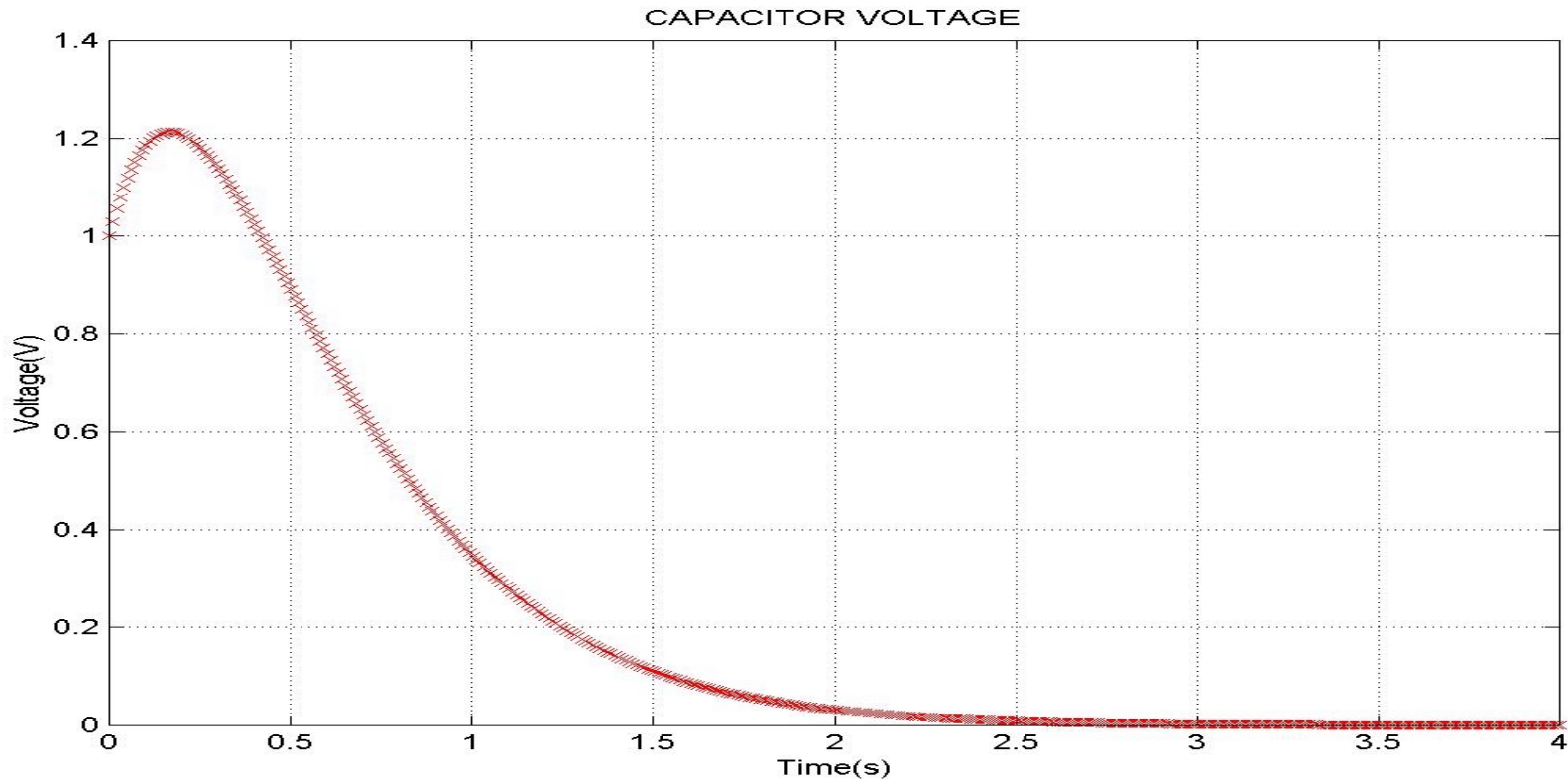
$\frac{d^2v}{dt^2}(t) + 6 \frac{dv}{dt}(t) + 9v(t) = 0$

Ch. Eq.: $s^2 + 6s + 9 = 0$



USING MATLAB TO VISUALIZE RESPONSE

```
%script6p9.m  
%displays the function  $v(t)=\exp(-3t)(1+6t)$   
tau=1/3;  
tend=ceil(10*tau);  
t=linspace(0,tend,400);  
vt=exp(-3*t).*(1+6*t);  
plot(t,vt,'rx'),grid, xlabel('Time(s)'), ylabel('Voltage(V)')  
title('CAPACITOR VOLTAGE')
```



LEARNING EXTENSION

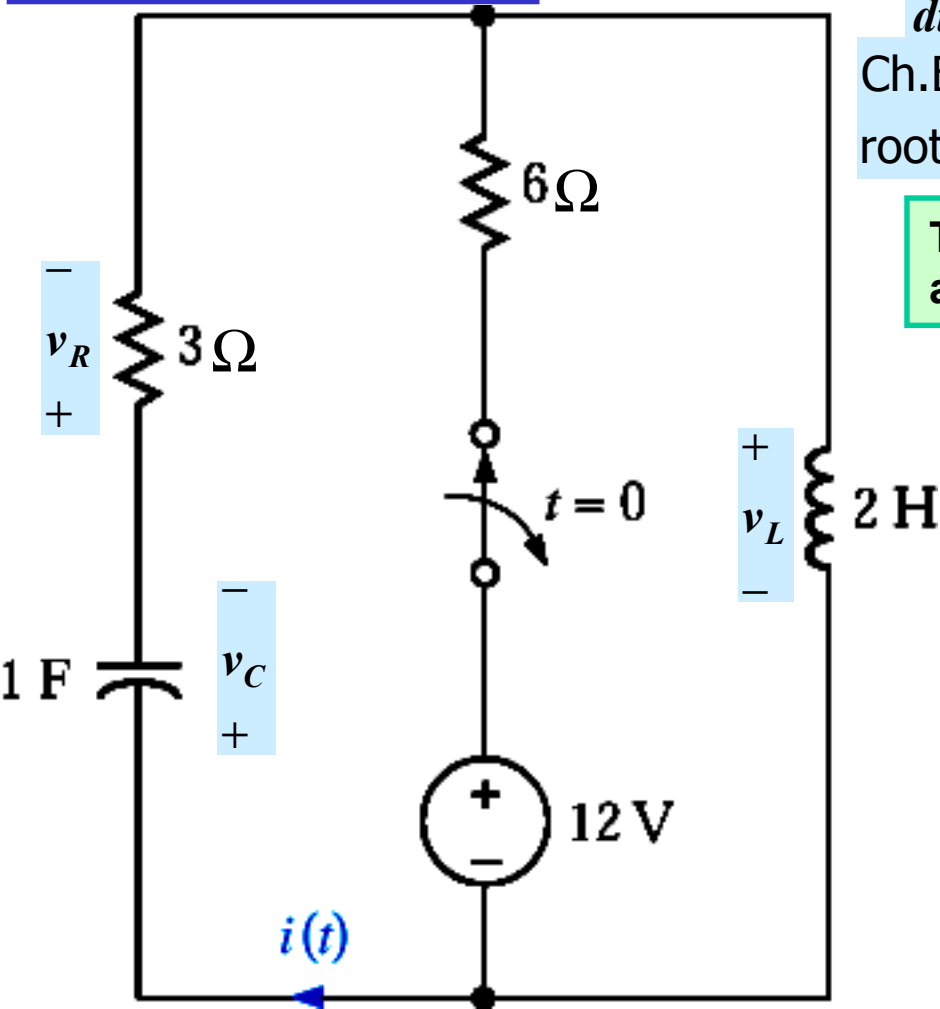
FIND $i(t), t > 0$

$$\frac{d^2 i}{dt^2}(t) + \frac{3}{2} \frac{di}{dt}(t) + \frac{1}{2} i(t) = 0$$

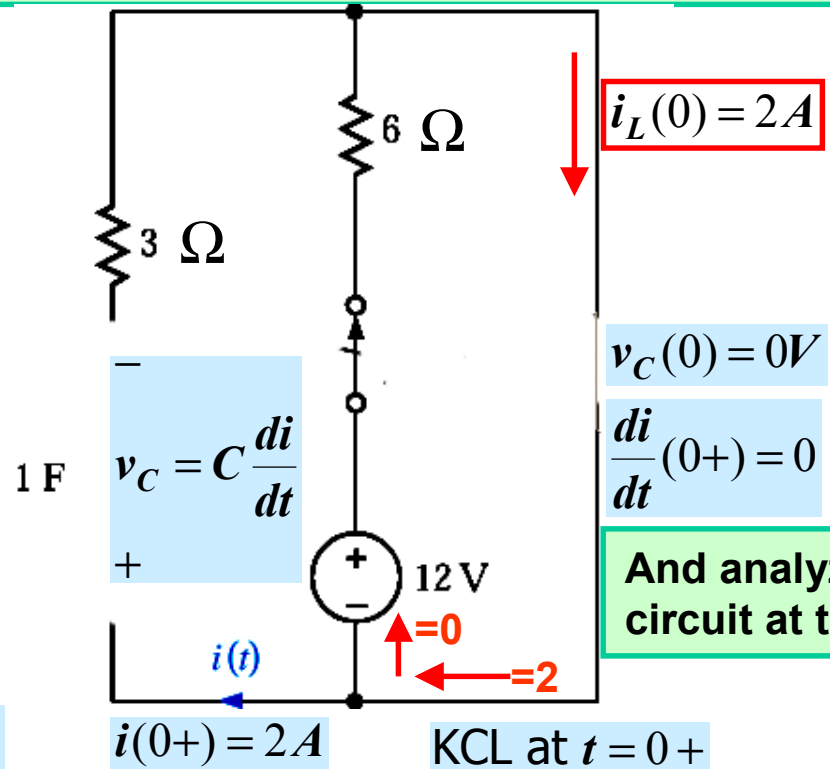
Ch.Eq.: $s^2 + 1.5s + 0.5 = 0$

roots: $s = -1, -0.5$

$$i(t) = K_1 e^{-t} + K_2 e^{-\frac{t}{2}}; t > 0$$



To find initial conditions use steady state analysis for $t < 0$



Once the switch opens the circuit is RLC series

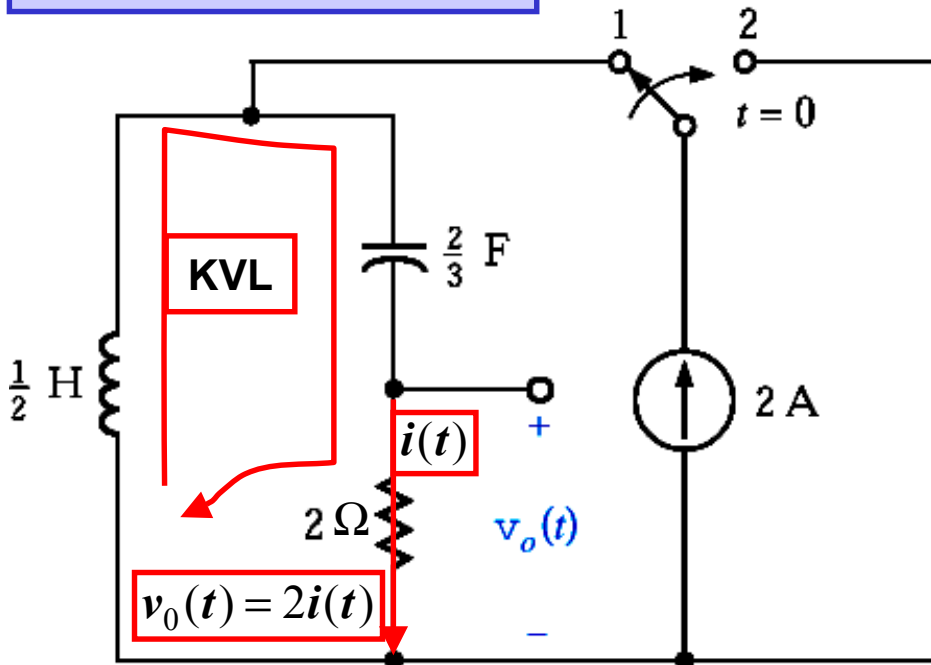
$$3i(t) + 2 \frac{di}{dt}(t) + v_C(0) + \int_0^t i(x) dx = 0$$

$$2 = K_1 + K_2$$

$$0 = -K_1 - \frac{1}{2} K_2$$

$$i(t) = -2e^{-t} + 4e^{-\frac{t}{2}}; t > 0$$

LEARNING EXTENSION FIND $v_0(t), t > 0$



For $t > 0$ the circuit is RLC series

$$\frac{1}{2} \frac{di}{dt}(t) + \frac{1}{2/3} \int_0^t i(x) dx + v_C(0) + 2i(t) = 0$$

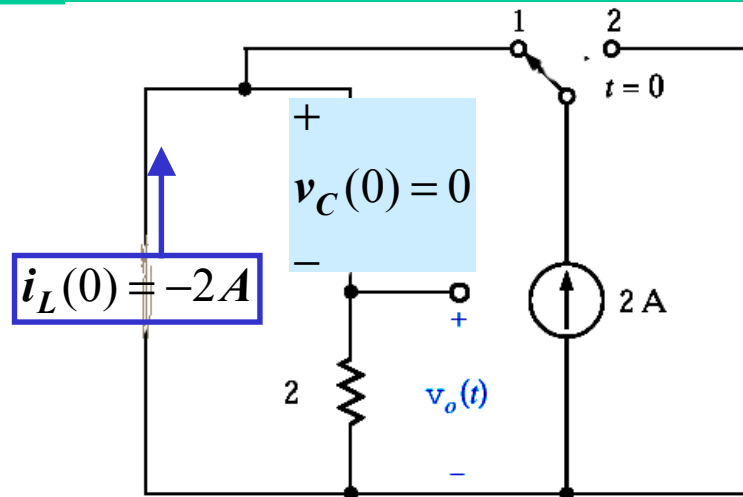
$$\frac{d^2 i}{dt^2}(t) + 4 \frac{di}{dt}(t) + 3i(t) = 0$$

Ch. Eq. : $s^2 + 4s + 3 = 0$

roots: $s = -1, -3$

$$i(t) = K_1 e^{-t} + K_2 e^{-3t}; t > 0$$

To find initial conditions we use steady state analysis for $t < 0$



And analyze circuit at $t = 0+$

$$i(0+) = -2 A$$

$$v_C(0+) = C \frac{di}{dt}(0+) = 0$$

$$i(0+) = 0 \Rightarrow K_1 + K_2 = -2$$

$$K_2 = 1$$

$$\frac{di}{dt}(0+) = 0 \Rightarrow -K_1 - 3K_2 = 0$$

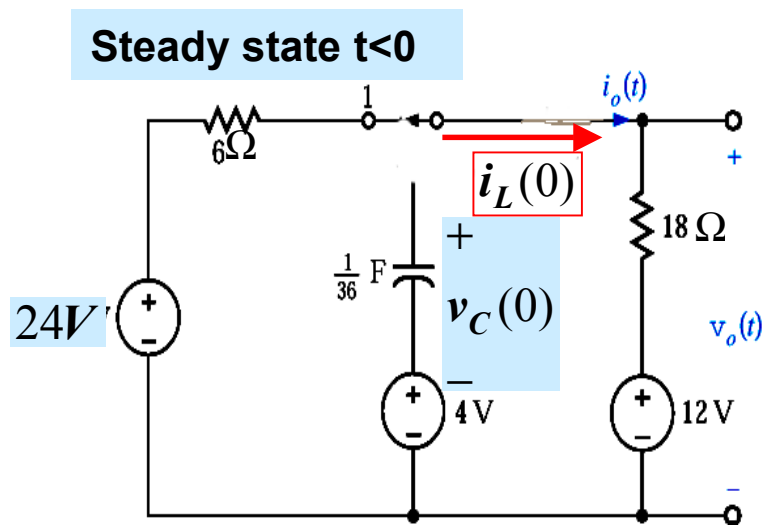
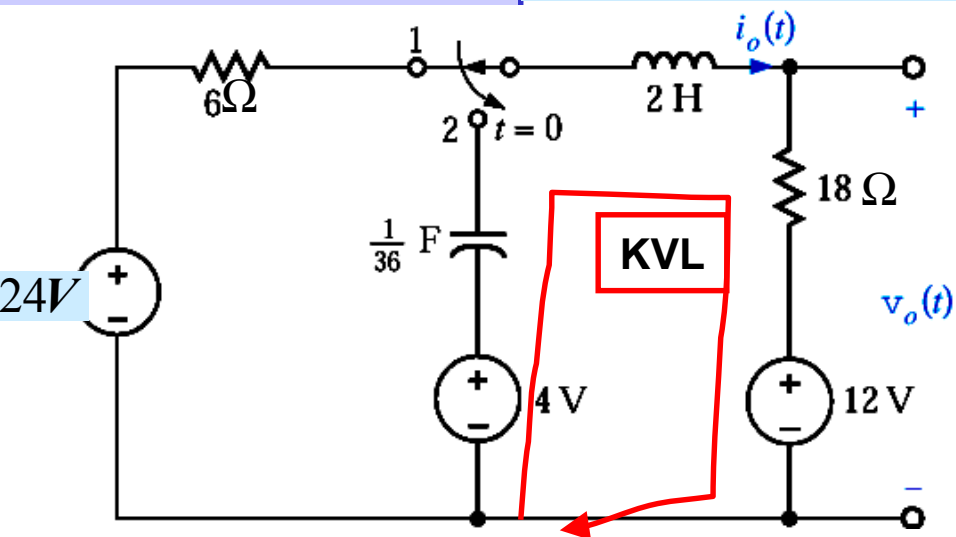
$$K_1 = -3$$

$$\therefore i(t) = -3e^{-t} + e^{-3t}; t > 0$$

$$v_0(t) = 2(-3e^{-t} + e^{-3t}); t > 0$$



LEARNING EXTENSION DETERMINE $i_0(t), v_0(t); t > 0$ $v_0(t) = 18i_0(t) + 12(V)$



Steady state $t < 0$

$v_C(0) = 0$ $i_L(0) = 0.5 A$

$$-4 + \frac{1}{1/36} \int_0^t i(x) dx + v_C(0) + 2 \frac{di}{dt}(t) + 18i(t) + 12 = 0$$

$$\frac{d^2 i}{dt^2}(t) + 9 \frac{di}{dt}(t) + 18i(t) = 0$$

Ch. Eq.: $s^2 + 9s + 18 = 0$
 roots: $s = -3, -6$

$$i_0(t) = K_1 e^{-3t} + K_2 e^{-6t}; t > 0$$

$$i_0(t) = -\frac{11}{6} e^{-3t} + \frac{14}{6} e^{-6t}; t > 0$$

Analysis at $t = 0+$

$$i_0(0+) = i_L(0+) = 0.5(A)$$

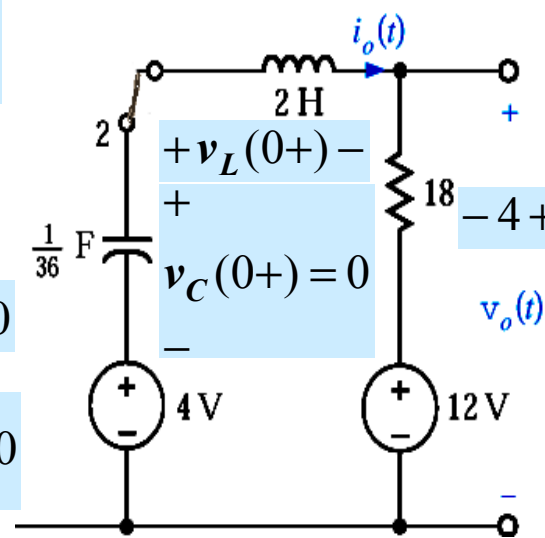
$$v_L(0+) = L \frac{di_L}{dt}(0+) = L \frac{di_0}{dt}(0+)$$

$$-4 + v_L(0+) + 18i_L(0+) + 12 = 0 \quad v_L(0+) = -17$$

$$\frac{di_0}{dt}(0+) = -17/2 = -3K_1 - 6K_2$$

$$i_0(0+) = 0.5 = K_1 + K_2$$

$$K_1 = -\frac{11}{6}; \quad K_2 = \frac{14}{6}$$



Second order

