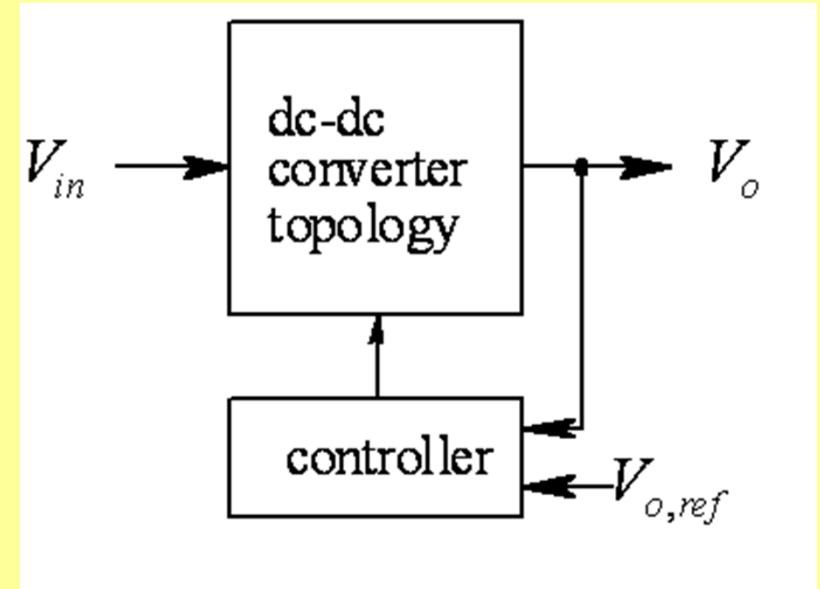
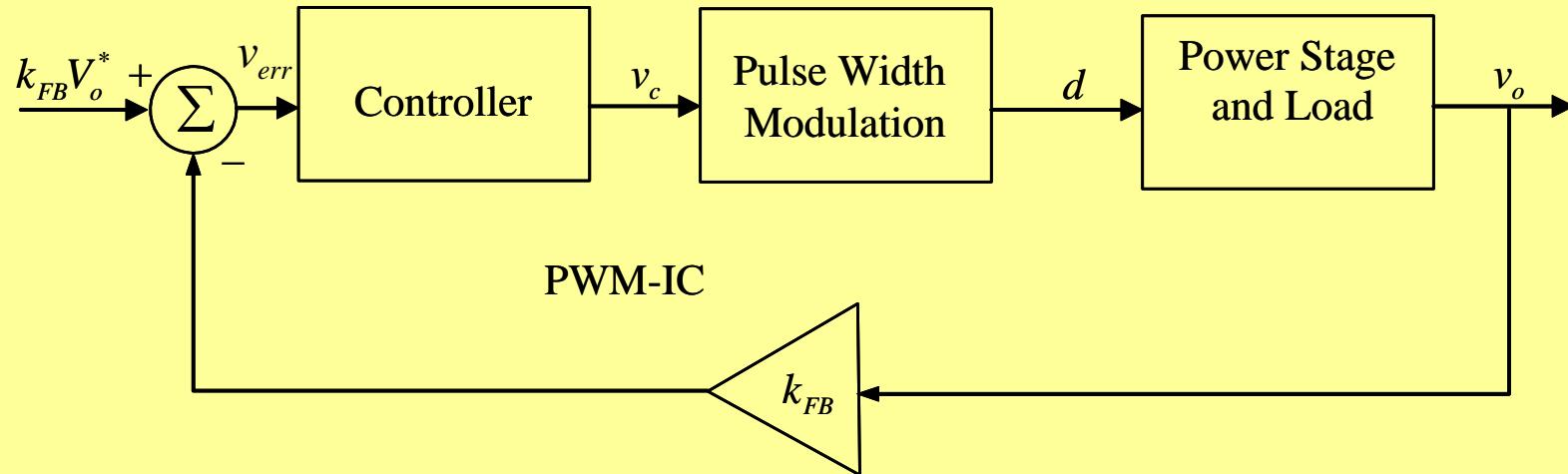


# Regulated DC Power Supply

- Voltage-Mode Control

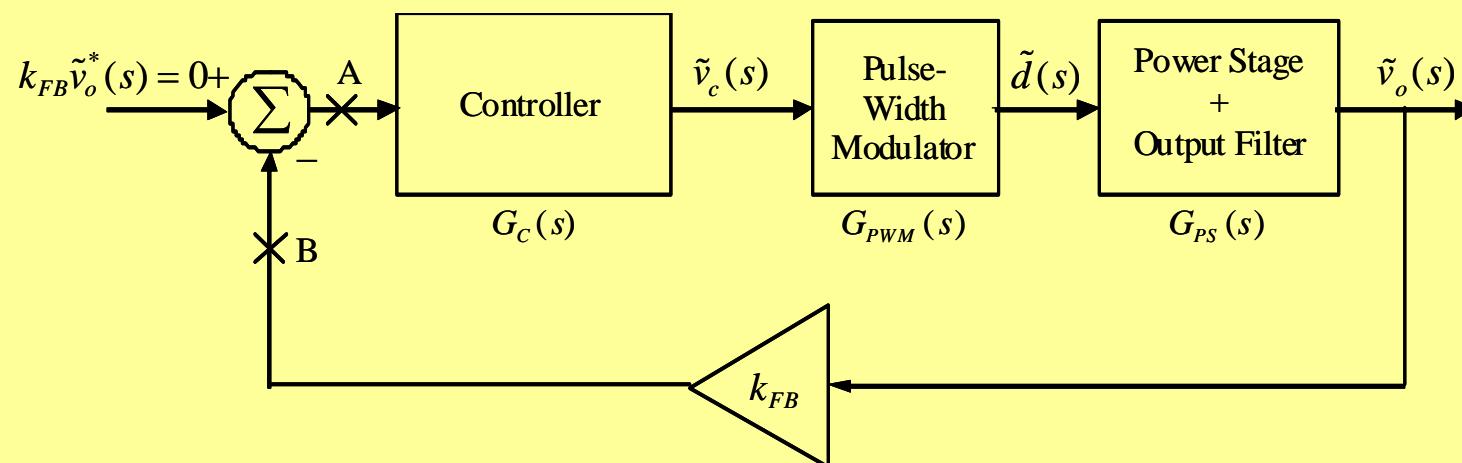


# APPLYING LINEAR CONTROL THEORY



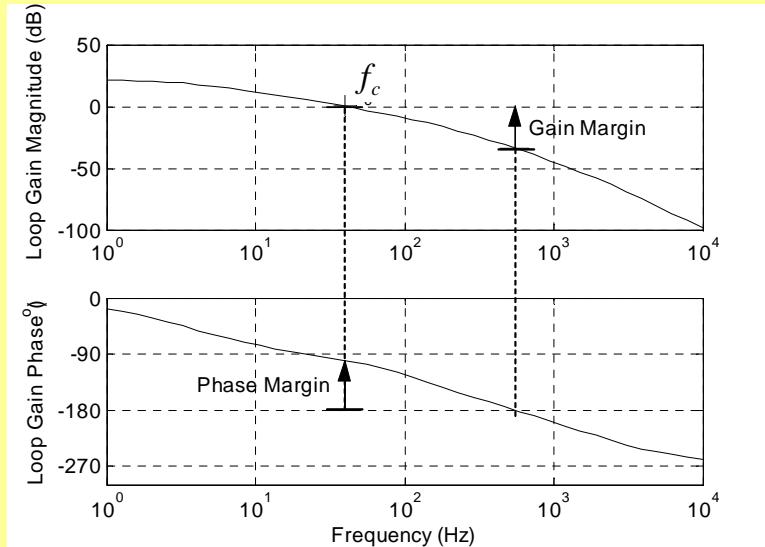
Small signal representation:

$$\begin{aligned}\bar{v}_o(t) &= V_o + \tilde{v}_o(t) \\ d(t) &= D + \tilde{d}(t) \\ v_c(t) &= V_c + \tilde{v}_c(t)\end{aligned}$$



Loop Transfer Function:

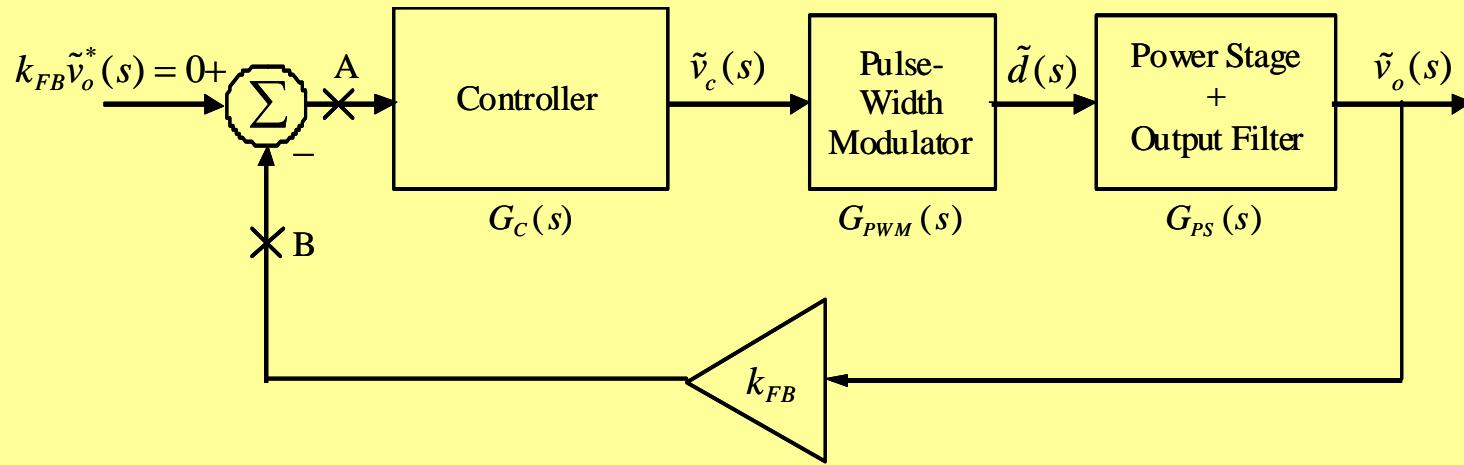
$$G_L(s) = G_C(s)G_{PWM}(s)G_{PS}(s)k_{FB}$$



Phase Margin:

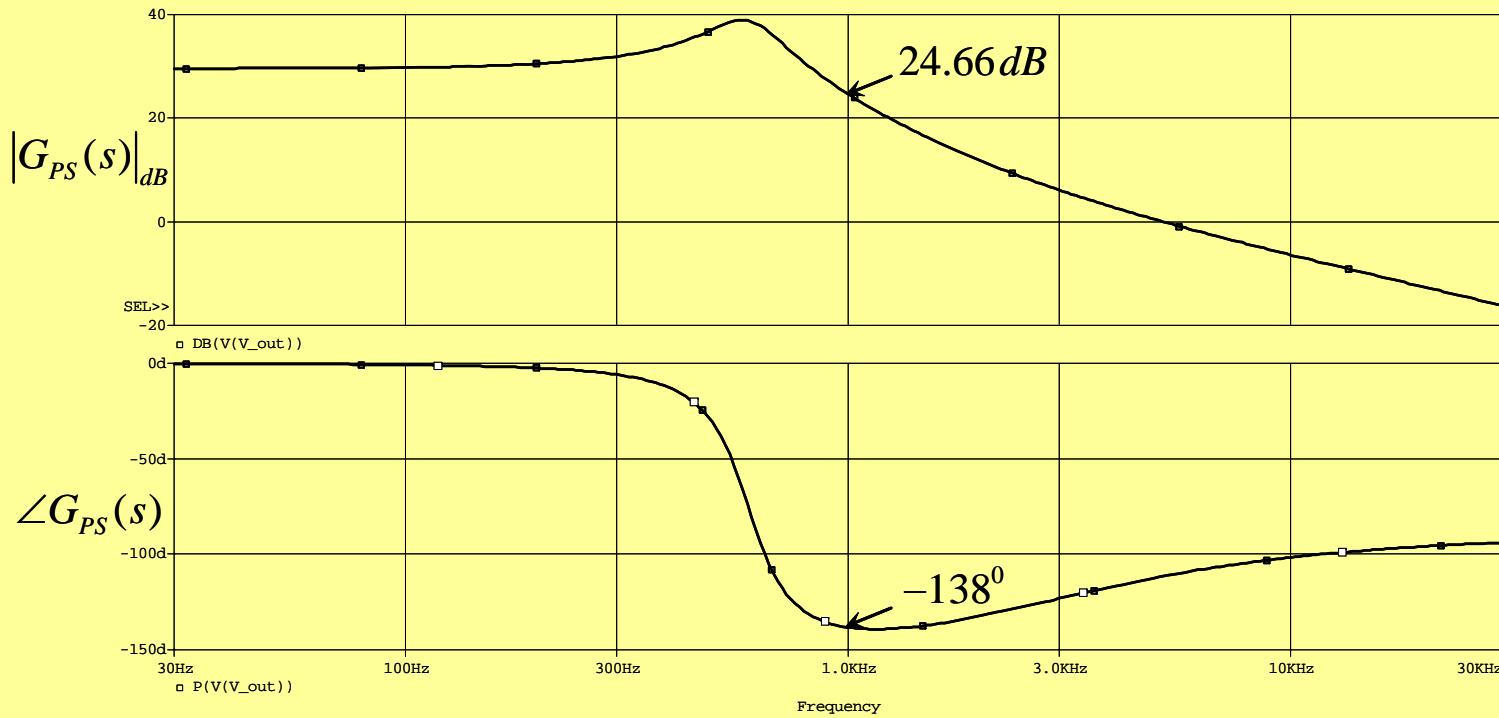
$$\phi_{PM} = \phi_L|_{f_c} - (-180^\circ) = \phi_L|_{f_c} + 180^\circ$$

## Form of the Controller Transfer Function:



$$G_c(s) = \frac{k_c}{s} \frac{(1 + s/\omega_z)^2}{(1 + s/\omega_p)^2}$$

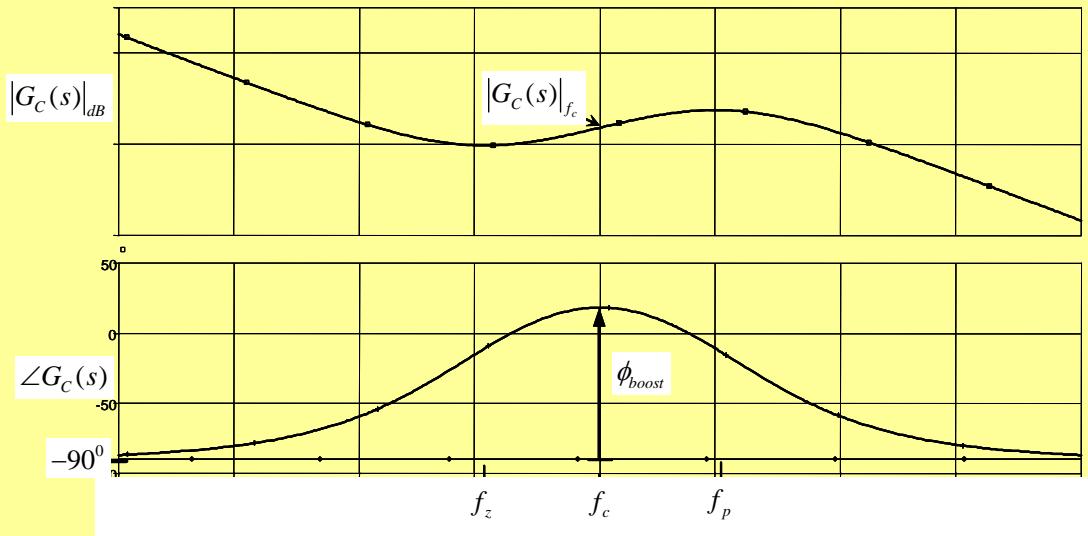
# Select the Crossover Frequency $f_c$



$$G_c(s) = \frac{k_c}{s} \frac{(1 + s/\omega_z)^2}{(1 + s/\omega_p)^2}$$

Calculate the needed Phase Boost:

$$G_c(s) = \frac{k_c}{s} \cdot \frac{(1 + s/\omega_z)^2}{(1 + s/\omega_p)^2}$$



$$\angle G_C(s) \Big|_{f_c} = -90^\circ + \phi_{boost}$$

$$\angle G_L(s) \Big|_{f_c} = \angle G_{PS}(s) \Big|_{f_c} + \angle G_C(s) \Big|_{f_c} = -180^\circ + \phi_{PM}$$

$$\phi_{boost} = -90^\circ + \phi_{PM} - \angle G_{PS}(s) \Big|_{f_c} \quad \sqrt{\frac{\omega_p}{\omega_z}} = \tan\left(45^\circ + \frac{\phi_{boost}}{4}\right)$$

$$\omega_c = \sqrt{\omega_z \omega_p}$$

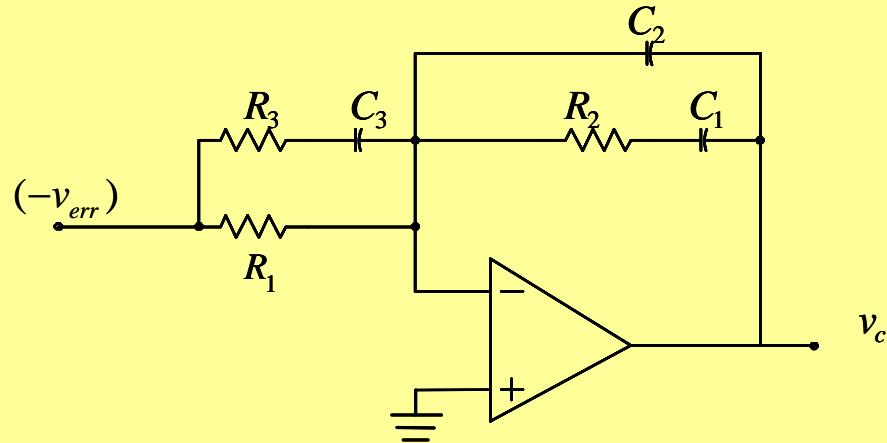
# Calculating the Controller Gain $k_c$

$$G_c(s) = \frac{k_c}{s} \cdot \frac{(1 + s/\omega_z)^2}{(1 + s/\omega_p)^2}$$

$$\left|G_L(s)\right|_{f_c} = \left|G_C(s)\right|_{f_c} \times \left|G_{PWM}(s)\right|_{f_c} \times \left|G_{PS}(s)\right|_{f_c} \times k_{FB} = 1$$

## Implementation of the controller by an op-amp

$$G_c(s) = \frac{k_c}{s} \frac{(1 + s/\omega_z)^2}{(1 + s/\omega_p)^2}$$



$$C_2 = \omega_z / (k_c \omega_p R_1)$$

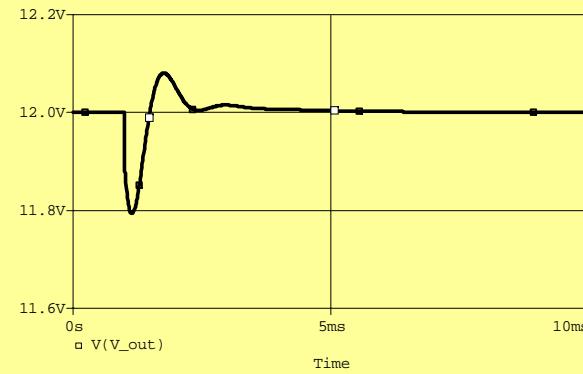
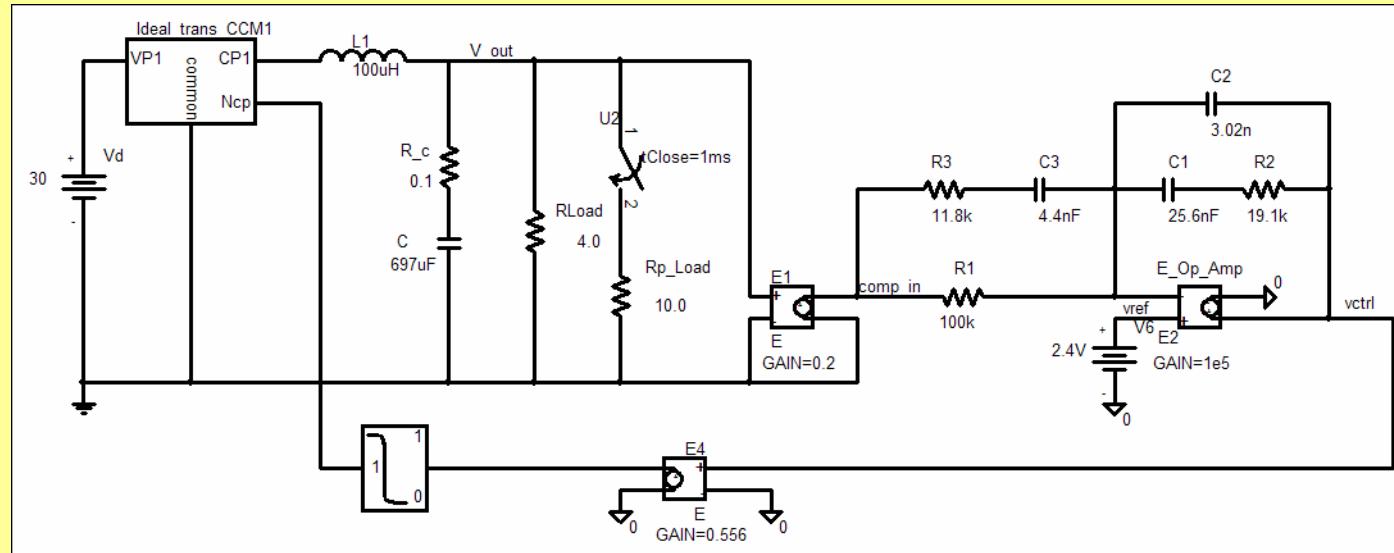
$$C_1 = C_2 (\omega_p / \omega_z - 1)$$

$$R_2 = 1 / (\omega_z C_1)$$

$$R_3 = R_1 / (\omega_p / \omega_z - 1)$$

$$C_3 = 1 / (\omega_p R_3)$$

## PSpice model of the Buck converter with voltage-mode control



# Summary

Regulated DC Power Supply

- Voltage-Mode Control