

MAGNETICALLY COUPLED NETWORKS

LEARNING GOALS

Mutual Inductance

Behavior of inductors sharing a common magnetic field

Energy Analysis

Used to establish relationship between mutual reluctance and self-inductance

The ideal transformer

Device modeling components used to change voltage and/or current levels

Safety Considerations

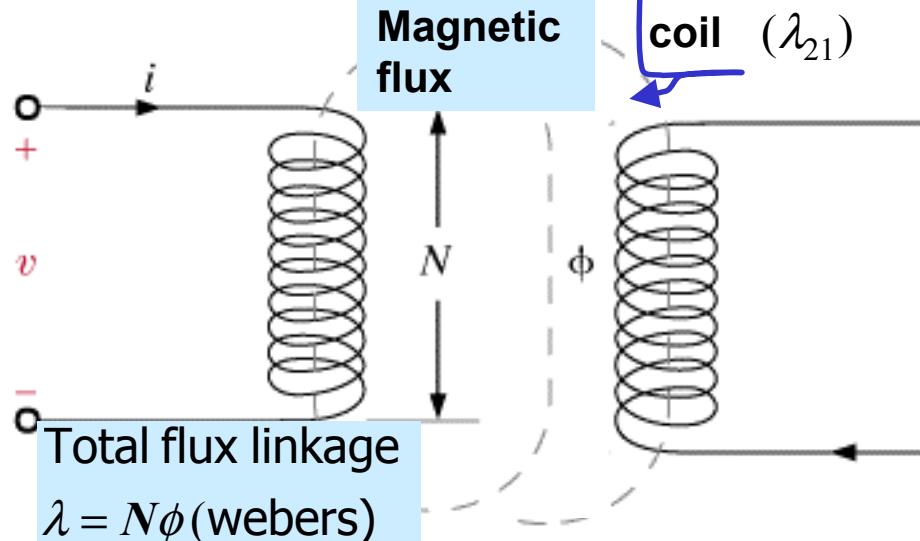
Important issues for the safe operation of circuits with transformers



GEAUX

MUTUAL INDUCTANCE

Overview of Induction Laws



If linkage is created by a current flowing through the coils...

$$\lambda = Li \quad (\text{Ampere's Law})$$

The voltage created at the terminals of the components is

$$v = L \frac{di}{dt} \quad (\text{Faraday's Induction Law})$$

What happens if the flux created by the current links to another coil?

One has the effect of mutual inductance

Assume n circuits interacting

$$\lambda_i = \sum_{j=1}^n \lambda_{ij}$$

λ_i = Total flux linking circuit i

λ_{ij} = Flux linking circuit i caused by a current in circuit j

For linear inductor models

$$\lambda_{ij} = L_{ij}i_j$$

L_{ii} = "self inductance" of circuit i

$L_{ij} = L_{ji}$ = Mutual inductance between circuits i and j

Special case $n=2$

$$\lambda_1 = L_{11}i_1 + L_{12}i_2$$

$$\lambda_2 = L_{21}i_1 + L_{22}i_2$$

Linear Model:

$$L_{12} = L_{21}$$

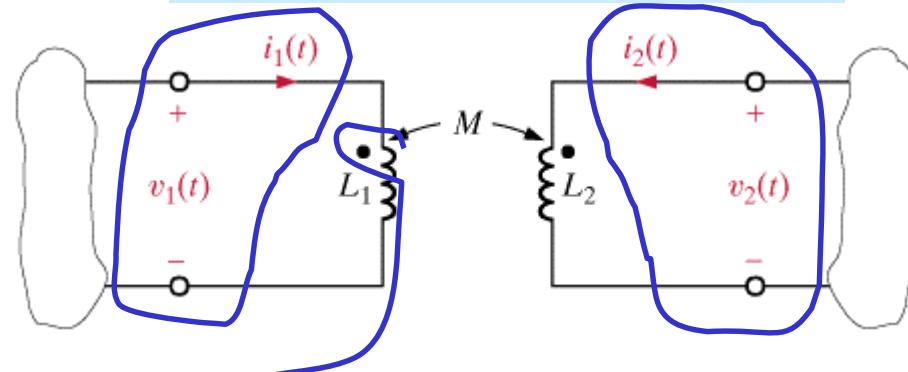
Simplify notation

$$L_1 \leftarrow L_{11}; L_2 \leftarrow L_{22}; M \leftarrow L_{12} = L_{21}$$

THE DOT CONVENTION

LEARNING EXAMPLE

Currents and voltages follow passive sign convention

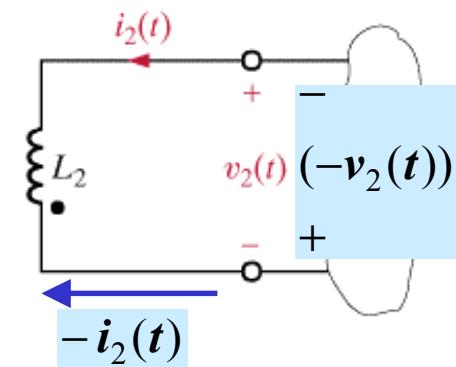
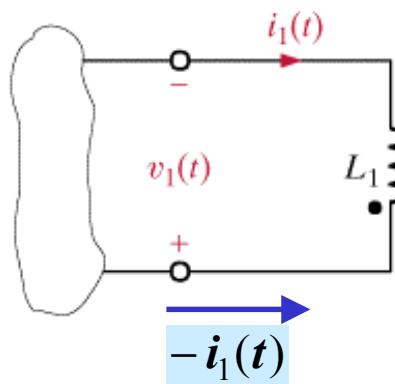


Flux 2 induced voltage has + at dot

$$v_1(t) = L_1 \frac{di_1}{dt}(t) + M \frac{di_2}{dt}(t)$$

$$v_2(t) = M \frac{di_1}{dt}(t) + L_2 \frac{di_2}{dt}(t)$$

For other cases change polarities or current directions to convert to this basic case



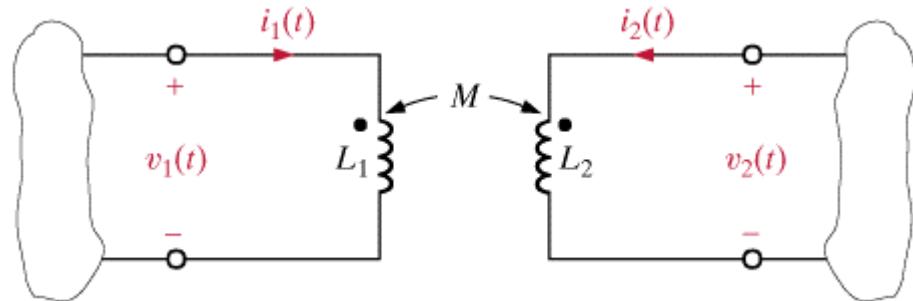
$$v_1(t) = L_1 \left(-\frac{di_1}{dt} \right) + M \left(-\frac{di_2}{dt} \right)$$

$$-v_2(t) = M \left(-\frac{di_1}{dt} \right) + L_2 \left(-\frac{di_2}{dt} \right)$$

$$v_1 = -L_1 \frac{di_1}{dt} - M \frac{di_2}{dt}$$

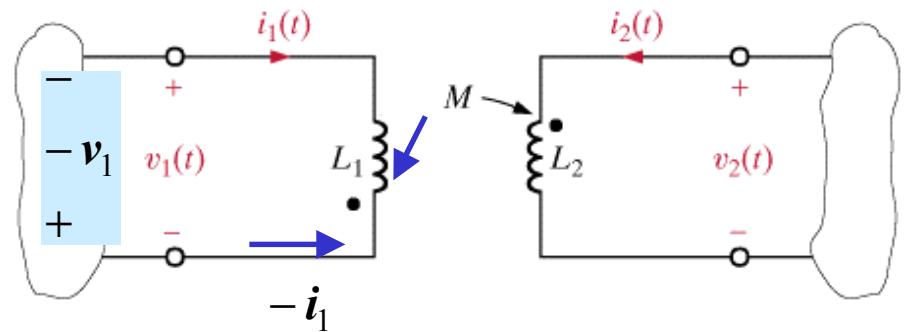
$$v_2 = M \frac{di_1}{dt} + L_2 \frac{di_2}{dt}$$

More on the dot convention



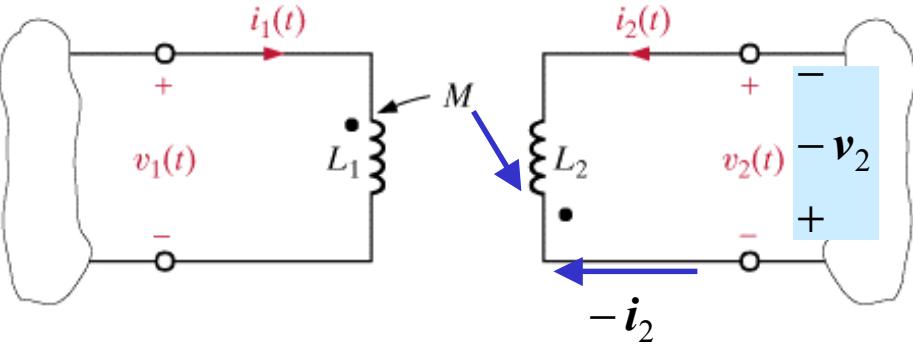
$$v_1(t) = L_1 \frac{di_1}{dt} + M \frac{di_2}{dt}$$

$$v_2(t) = M \frac{di_1}{dt} + L_2 \frac{di_2}{dt}$$



$$-v_1 = -L_1 \frac{di_1}{dt} + M \frac{di_2}{dt}$$

$$v_2 = -M \frac{di_1}{dt} + L_2 \frac{di_2}{dt}$$



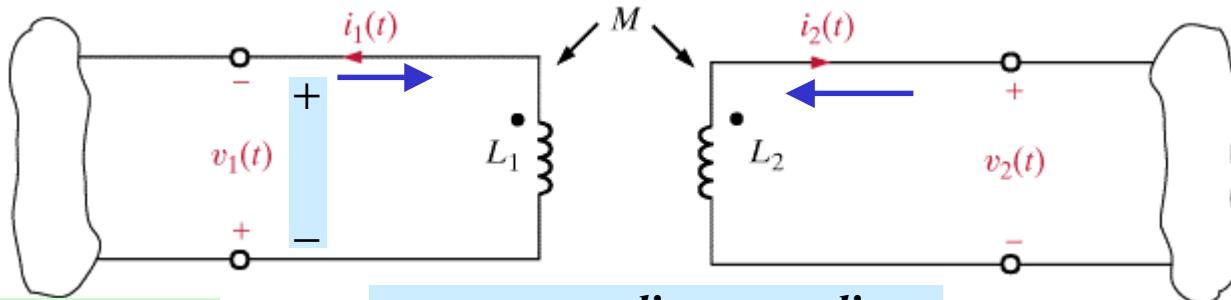
$$v_1 = L_1 \frac{di_1}{dt} - M \frac{di_2}{dt}$$

$$-v_2 = M \frac{di_1}{dt} - L_2 \frac{di_2}{dt}$$

Equivalent to a negative mutual inductance

LEARNING EXTENSION

Write the equations for $v_1(t), v_2(t)$



Convert to basic case

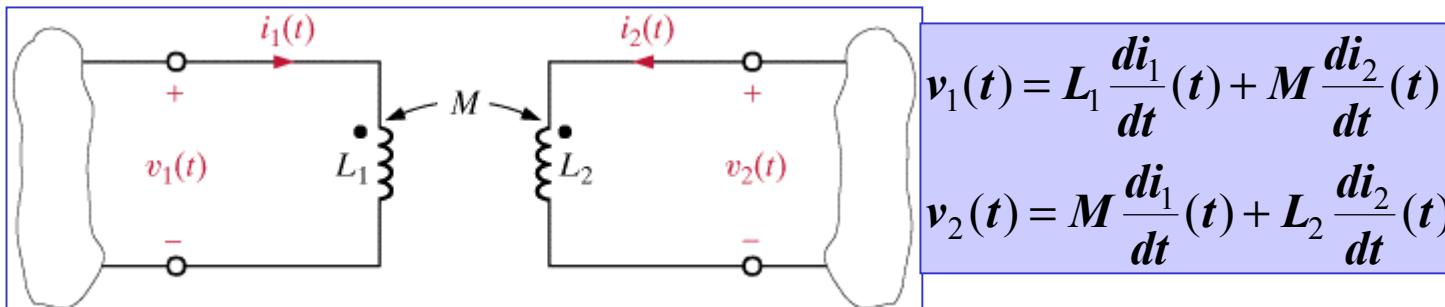
$$-v_1(t) = -L_1 \frac{di}{dt}(t) - M \frac{di_2}{dt}(t)$$

$$v_2(t) = -M \frac{di_1}{dt}(t) - L_2 \frac{di_2}{dt}(t)$$

$$v_1(t) = L_1 \frac{di}{dt}(t) + M \frac{di_2}{dt}(t)$$

$$v_2(t) = -M \frac{di_1}{dt}(t) - L_2 \frac{di_2}{dt}(t)$$

PHASORS AND MUTUAL INDUCTANCE



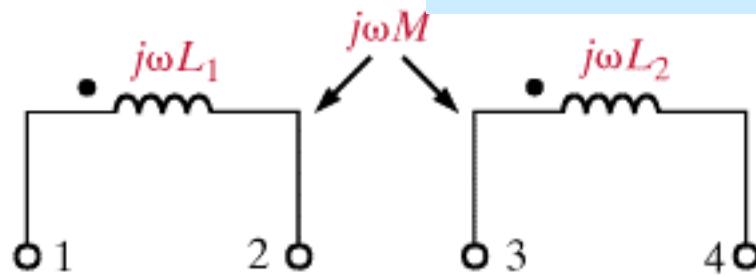
Assuming complex exponential sources

$$\begin{aligned} V_1 &= j\omega L_1 I_1 + j\omega M I_2 \\ V_2 &= j\omega M I_1 + j\omega L_2 I_2 \end{aligned}$$

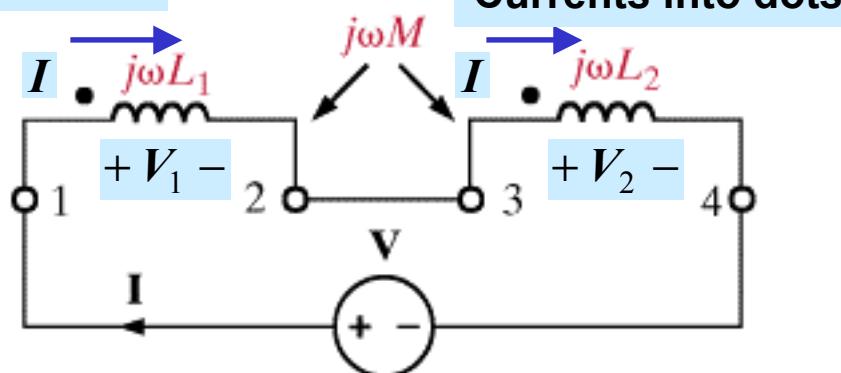
Phasor model for mutually coupled linear inductors

LEARNING EXAMPLE

The coupled inductors can be connected in four different ways.
Find the model for each case



CASE I



Currents into dots

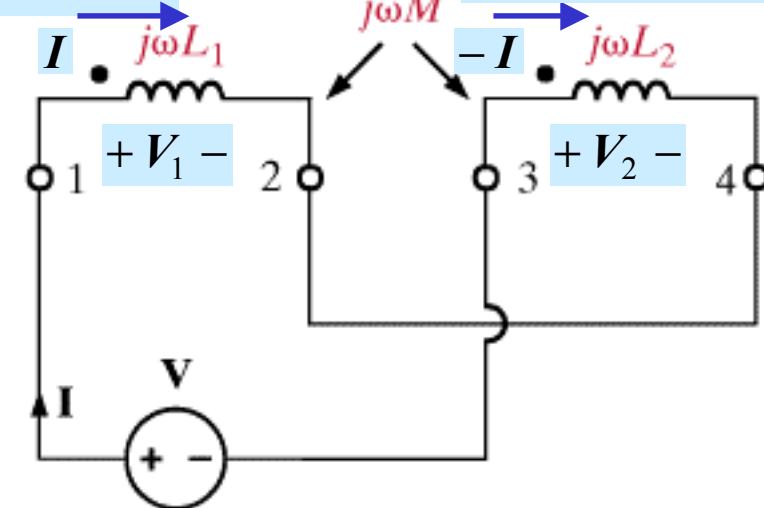
$$V = V_1 + V_2$$

$$V_1 = j\omega L_1 I + j\omega M I$$

$$V_2 = j\omega M I + j\omega L_2 I$$

$$V = j\omega(L_1 + L_2 + 2M)I = j\omega L_{eq} I$$

CASE 2



Currents into dots

$$V = V_1 - V_2$$

$$V_1 = j\omega L_1 I - j\omega M I$$

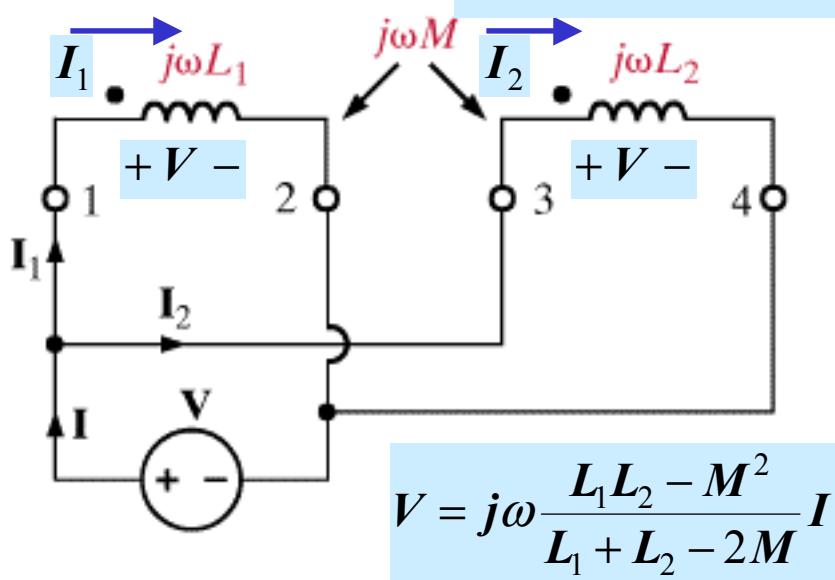
$$V_2 = j\omega M I - j\omega L_2 I$$

$$V = j\omega(L_1 - 2M + L_2)I$$

L_{eq}

$L_{eq} \geq 0$ imposes a physical constraint
on the value of M

CASE 3



$$I = I_1 + I_2 \Rightarrow I_2 = I - I_1$$

$$V = j\omega L_1 I_1 + j\omega M I_2$$

$$V = j\omega M I_1 + j\omega L_2 I_2$$

$$V = j\omega L_1 I_1 + j\omega M(I - I_1)$$

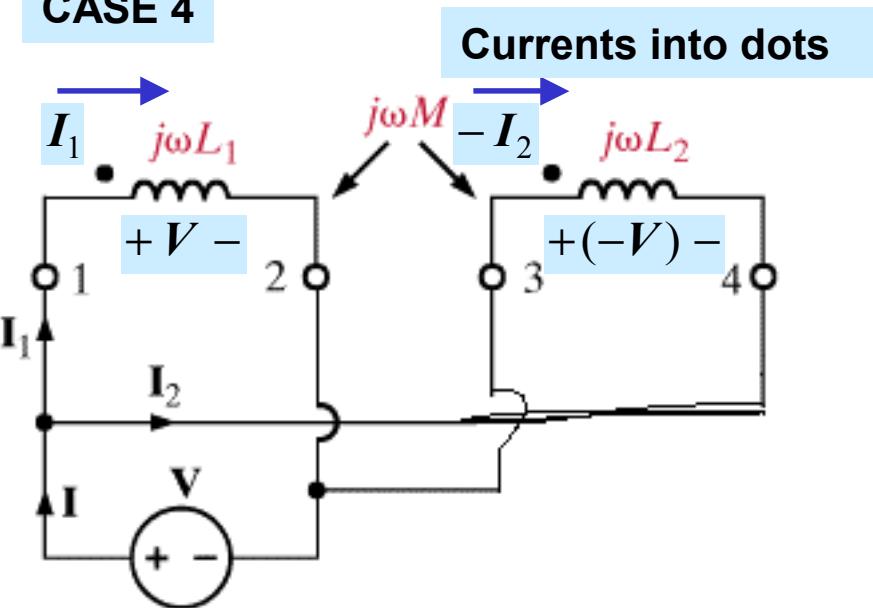
$$V = j\omega M I_1 + j\omega L_2(I - I_1)$$

$$V = j\omega(L_1 - M)I_1 + j\omega M I \quad \times/(L_2 - M)$$

$$V = -j\omega(L_2 - M)I_1 + j\omega L_2 I \quad \times/(L_1 - M)$$

$$(L_1 + L_2 - 2M)V = j\omega(M(L_2 - M) + L_2(L_1 - M))I$$

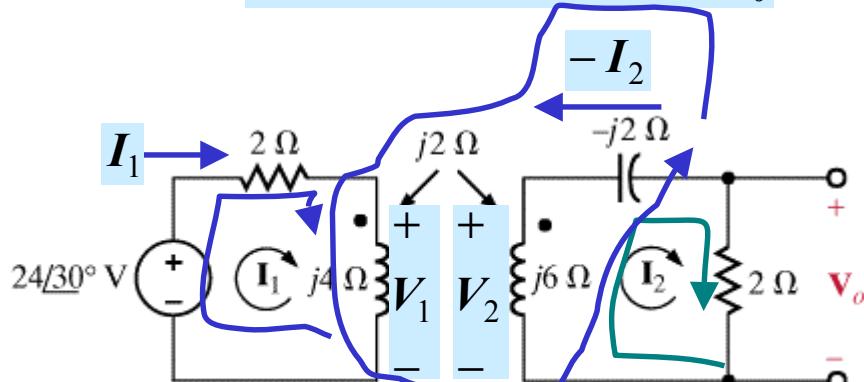
CASE 4



$$V = \frac{L_1 L_2 - M^2}{L_1 + L_2 + 2M} I$$

LEARNING EXAMPLE

FIND THE VOLTAGE V_0



KVL: $24\angle 30^\circ = 2I_1 + V_1$

V_s

KVL: $-V_2 - j2I_2 + 2I_2 = 0$

MUTUAL INDUCTANCE CIRCUIT

$$V_1 = j4I_1 + j2(-I_2)$$

$$V_2 = j2I_1 + j6(-I_2)$$

$$V_0 = 2I_2$$

$$V_s = (2 + j4)I_1 - j2I_2 \quad \times / j2$$

$$0 = -j2I_1 + (2 - j2 + j6)I_2 \quad \times / 2 + j4$$

$$j2V_s = (4 + (2 + j4)^2)I_2$$

$$I_2 = \frac{j2V_s}{-8 + j16} \times \frac{-j}{-j} = \frac{2V_s}{16 + 8j}$$

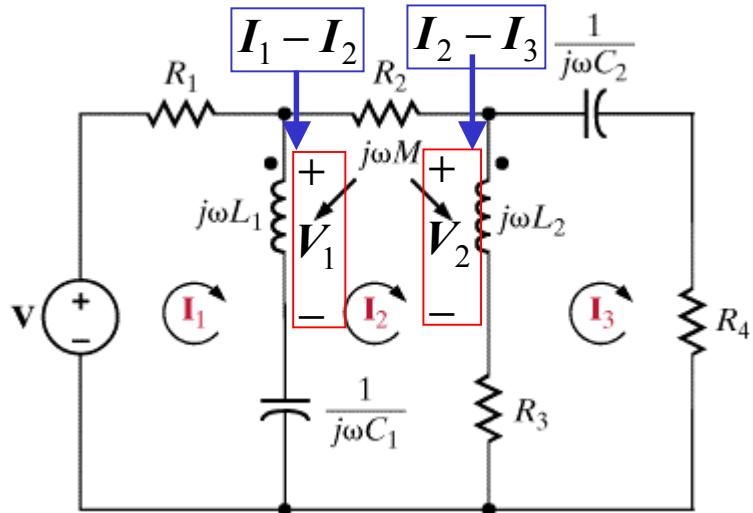
$$V_0 = 2I_2 = \frac{V_s}{4 + 2j} = \frac{24\angle 30^\circ}{4.47\angle 26.57^\circ} = 5.37\angle 3.42^\circ$$

1. Coupled inductors. Define their voltages and currents

2. Write loop equations in terms of coupled inductor voltages

3. Write equations for coupled inductors

4. Replace into loop equations and do the algebra



1. Define variables for coupled inductors

2. Write loop equations in terms of coupled inductor voltages

$$V = R_1 I_1 + V_1 + \frac{I_1 - I_2}{j\omega C_1}$$

$$-V_1 + R_2 I_2 + V_2 + R_3 (I_2 - I_3) + \frac{I_2 - I_1}{j\omega C_1} = 0$$

$$-V_2 + \frac{I_3}{j\omega C_2} + R_4 I_3 + R_3 (I_3 - I_2) = 0$$

3. Write equations for coupled inductors

$$V_1 = j\omega L_1 (I_1 - I_2) + j\omega M (I_2 - I_3)$$

$$V_2 = j\omega M (I_1 - I_2) + j\omega L_2 (I_2 - I_3)$$

4. Replace into loop equations and rearrange terms

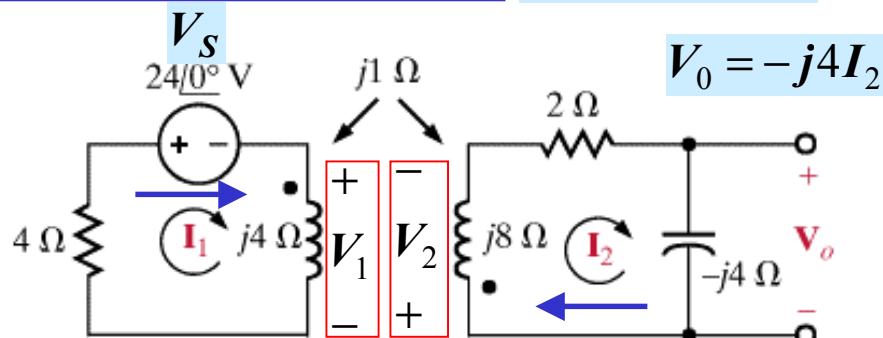
$$V = \left(R_1 + j\omega L_1 + \frac{1}{j\omega C_1} \right) I_1 - \left(j\omega L_1 - j\omega M + \frac{1}{j\omega C_1} \right) I_2 - j\omega M I_3$$

$$0 = - \left(j\omega L_1 - j\omega M + \frac{1}{j\omega C_1} \right) I_1 + \left(j\omega L_2 - j\omega M + R_2 - j\omega M + j\omega L_2 + R_3 + \frac{1}{j\omega C_1} \right) I_2 - (-j\omega M + j\omega L_2 + R_3) I_3$$

$$0 = -j\omega M I_1 - (j\omega L_2 - j\omega M + R_3) I_2 + \left(j\omega L_2 + \frac{1}{j\omega C_2} + R_4 + R_3 \right) I_3$$

LEARNING EXTENSION

FIND I_1, I_2, V_0



$$V_0 = -j4I_2$$

$$I_2 = \frac{jV_S}{-7 + 24j} \times \frac{-j}{-j} = \frac{24\angle 0^\circ}{24 + 7j} = \frac{24\angle 0^\circ}{25\angle 16.26^\circ}$$

$$I_2 = 0.96\angle -16.26^\circ(A)$$

$$jI_1 + (2 + j4)I_2 = 0 / \times j \Rightarrow I_1 = j(2 + j4)I_2$$

$$I_1 = 1\angle 90^\circ \times 4.47\angle 63.43^\circ \times 0.96\angle -16.26^\circ$$

$$I_1 = 4.29\angle 137.17^\circ(A)$$

$$V_0 = -j4I_2 = 1\angle -90^\circ \times 4 \times 0.96\angle -16.26^\circ$$

$$V_0 = 3.84\angle -106.26^\circ(V)$$

1. Define variables for coupled inductors

Voltages in Volts
Impedances in Ohms
Currents in ___

2. Loop equations

$$V_S + V_1 + 4I_1 = 0$$

$$V_2 + (2 - j4)I_2 = 0$$

3. Coupled inductors equations

$$V_1 = j4I_1 + jI_2$$

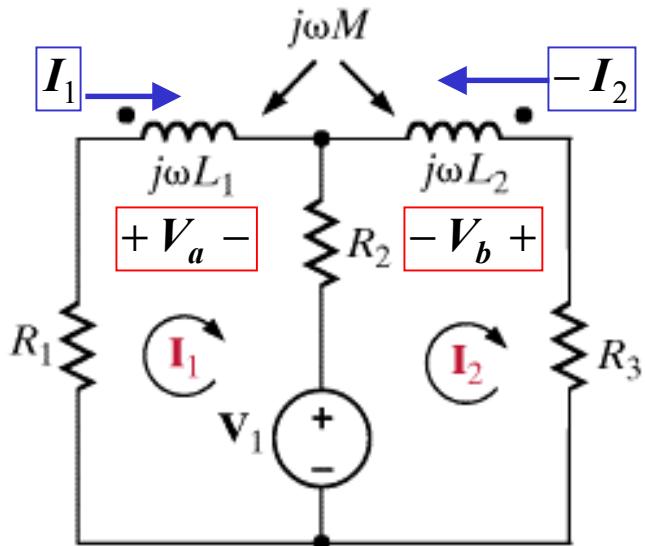
$$V_2 = jI_1 + j8I_2$$

4. Replace and rearrange

$$(4 + j4)I_1 + jI_2 = -V_S \quad \times / -j$$

$$jI_1 + (2 + j4)I_2 = 0 \quad \times / (4 + j4)$$

$$(1 + 8(1 + j)(1 + 2j))I_2 = jV_S$$



$$(R_1 + R_2 + j\omega L_1)I_1 - (R_2 + j\omega M)I_2 = -V_1$$

$$-(R_2 + j\omega M)I_1 + (R_2 + R_3 + j\omega L_2)I_2 = V_1$$

1. Define variables for coupled inductors

2. Loop equations in terms of inductor voltages

$$V_a + R_2(I_1 - I_2) + V_1 + R_1 I_1 = 0$$

$$-V_b + R_3 I_2 - V_1 + R_2(I_2 - I_1) = 0$$

3. Equations for coupled inductors

$$V_a = j\omega L_1 I_1 + j\omega M(-I_2)$$

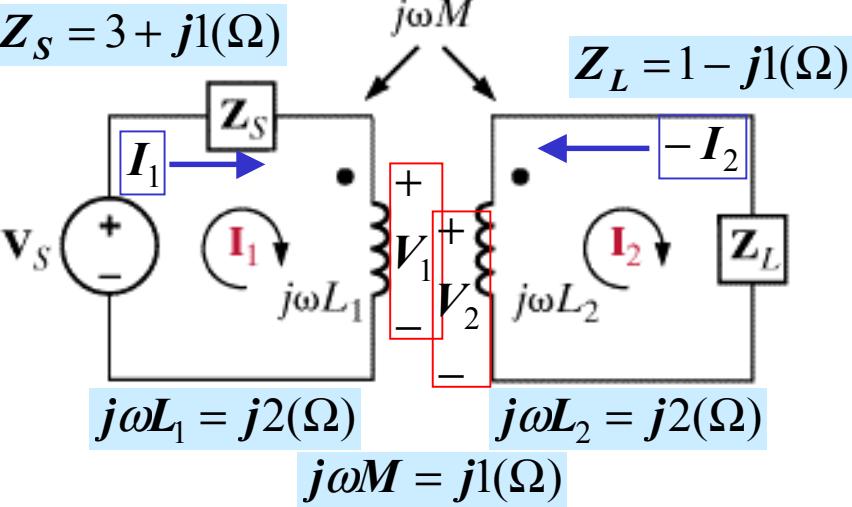
$$V_b = j\omega M I_1 + j\omega L_2(-I_2)$$

4. Replace into loop equations and rearrange

LEARNING EXAMPLE

DETERMINE IMPEDANCE SEEN BY THE SOURCE

$$Z_i = \frac{V_s}{I_1}$$



1. Variables for coupled inductors

2. Loop equations in terms of coupled inductors voltages

$$\begin{aligned} Z_S I_1 + V_1 &= V_s \\ -V_2 + Z_L I_2 &= 0 \end{aligned}$$

3. Equations for coupled inductors

$$\begin{aligned} V_1 &= j\omega L_1 I_1 + j\omega M(-I_2) \\ V_2 &= j\omega M I_1 + j\omega L_2(-I_2) \end{aligned}$$

4. Replace and do the algebra

$$\begin{aligned} (Z_S + j\omega L_1)I_1 - (j\omega M)I_2 &= V_s \quad \times / (Z_L + j\omega L_2) \\ -(j\omega M)I_1 + (Z_L + j\omega L_2)I_2 &= 0 \quad \times / j\omega M \end{aligned}$$

$$\begin{aligned} ((Z_S + j\omega L_1)(Z_L + j\omega L_2) - (j\omega M)^2)I_1 \\ = (Z_L + j\omega L_2)V_s \end{aligned}$$

$$Z_i = \frac{V_s}{I_1} = (Z_S + j\omega L_1) - \frac{(j\omega M)^2}{Z_L + j\omega L_2}$$

$$Z_i = 3 + j3 - \frac{(j1)^2}{1 + j1} = 3 + j3 + \frac{1}{1 + j} \times \frac{1 - j}{1 - j}$$

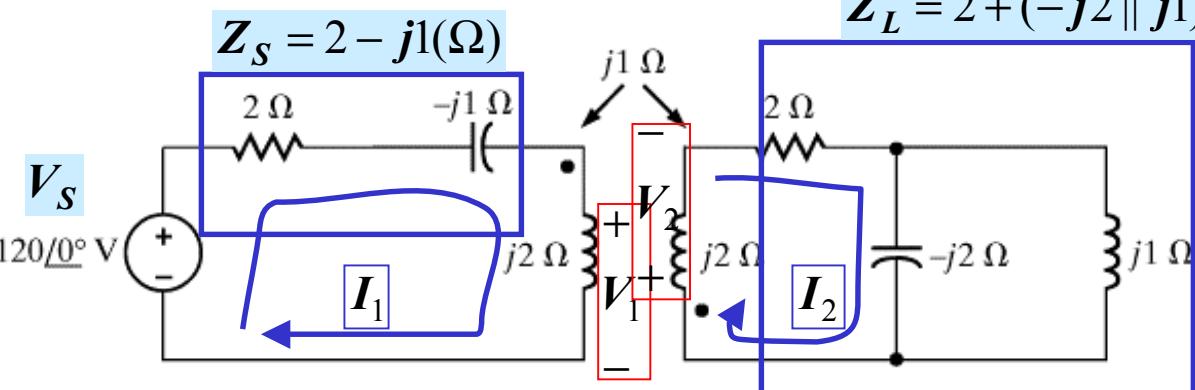
$$Z_i = 3 + j3 + \frac{1 - j}{2} = 3.5 + j2.5(\Omega)$$

$$Z_i = 4.30 \angle 35.54^\circ(\Omega)$$

WARNING: This is NOT a phasor

LEARNING EXTENSION

DETERMINE IMPEDANCE SEEN BY THE SOURCE



$$Z_L = 2 + \frac{2}{-j} = 2 + 2j(\Omega)$$

1. Variables for coupled inductors

2. Loop equations

$$V_1 + Z_S I_1 = V_S$$

$$V_2 + Z_L I_2 = 0$$

3. Equations for coupled inductors

$$V_1 = j\omega L_1 I_1 + j\omega M I_2$$

$$V_2 = j\omega M I_1 + j\omega L_2 I_2$$

4. Replace and do the algebra

One can choose directions for currents.

If I₂ is reversed one gets the same equations than in previous example.

Solution for I₁ must be the same and expression for impedance must be the same

$$Z_i = \frac{V_S}{I_1} = (Z_S + j\omega L_1) - \frac{(j\omega M)^2}{Z_L + j\omega L_2}$$

$$Z_i = [(2 - j1) + j2] - \frac{(j1)^2}{(2 + 2j) + 2j} = (2 + j) + \frac{1}{2(1 + 2j)} \times \frac{(1 - 2j)}{(1 - 2j)}$$

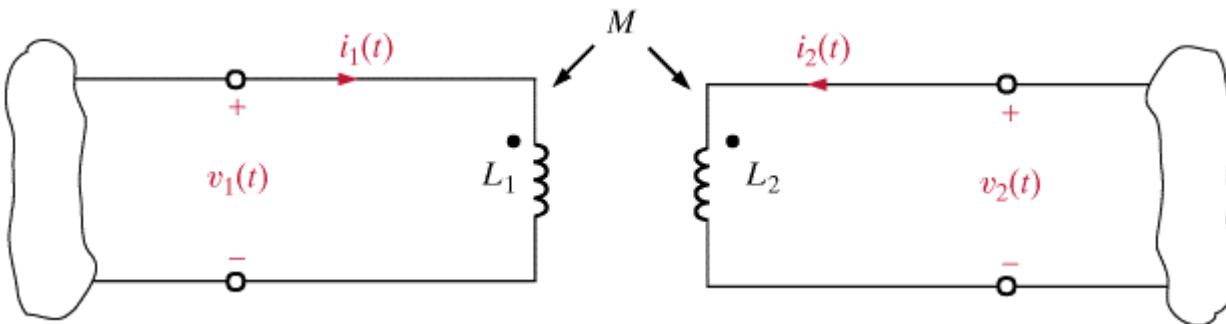
$$Z_i = 2 + j + \frac{1 - 2j}{2(1 + 2^2)} = 2.1 + 0.8j(\Omega)$$

$$Z_i = 2.25 \angle 20.85^\circ (\Omega)$$



ENERGY ANALYSIS

We determine the total energy stored in a coupled network



This development is different from the one in the book. But the final result is obviously the same

EQUATIONS FOR COUPLED INDUCTORS

$$v_1(t) = L_1 \frac{di_1}{dt} \pm M \frac{di_2}{dt} \quad \times / i_1(t)$$

$$v_2(t) = \pm M \frac{di_1}{dt} + L_2 \frac{di_2}{dt} \quad \times / i_2(t)$$

TOTAL POWER SUPPLIED TO NETWORK

$$p_T(t) = v_1(t)i_1(t) + v_2(t)i_2(t)$$

$$p_T(t) = L_1 i_1(t) \frac{di_1}{dt} \pm M i_1(t) \frac{di_2}{dt}$$

$$\pm M \frac{di_1}{dt} i_2(t) + L_2 i_2(t) \frac{di_2}{dt}$$

$\frac{1}{2} \frac{di_1^2}{dt}(t)$	$M \frac{di_1 i_2}{dt}(t)$
$\frac{1}{2} \frac{di_2^2}{dt}(t)$	

$$p_T(t) = \frac{d}{dt} \left(\frac{1}{2} L_1 i_1^2(t) \pm M i_1(t) i_2(t) + \frac{1}{2} L_2 i_2^2(t) \right) \int_{-\infty}^t$$

$$w(t) = \frac{1}{2} L_1 i_1^2(t) \pm M i_1(t) i_2(t) + \frac{1}{2} L_2 i_2^2(t)$$

$$+ \frac{1}{2} \frac{M^2}{L_2} i_1^2(t) - \frac{1}{2} \frac{M^2}{L_2} i_1^2(t)$$

$$w(t) = \frac{1}{2} \left(L_1 - \frac{M^2}{L_2} \right) i_1^2(t) + \frac{1}{2} \left(L_2 i_2(t) \pm \frac{M}{\sqrt{L_2}} i_1(t) \right)^2$$

$$w(t) \geq 0 \iff L_1 - \frac{M^2}{L_2} \geq 0 \iff M \leq \sqrt{L_1 L_2}$$

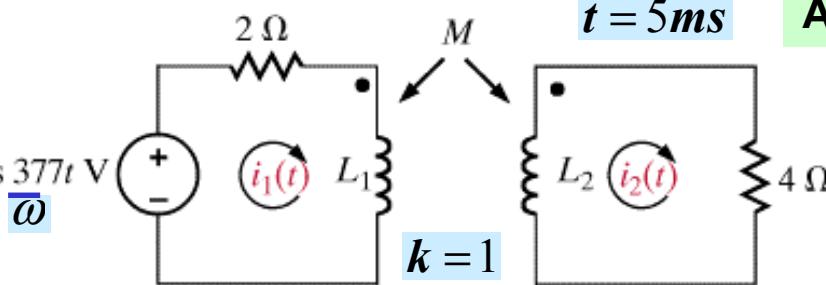
$$k = \frac{M}{\sqrt{L_1 L_2}}$$

Coefficient of coupling

GEAUX

LEARNING EXAMPLE

Compute the energy stored in the mutually coupled inductors



$$L_1 = 2.653\text{mH}, L_2 = 10.61\text{mH}$$

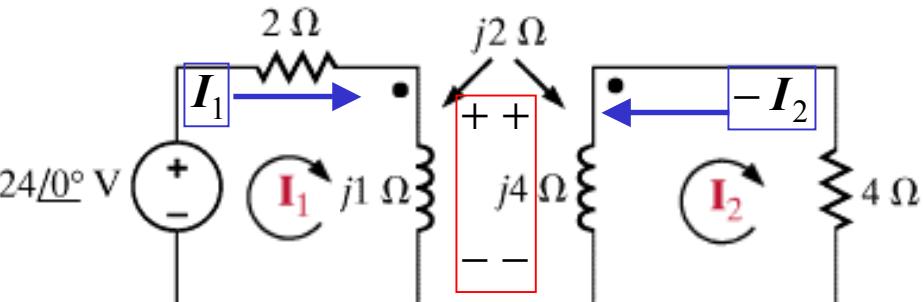
$$w(t) = \frac{1}{2}L_1 i_1^2(t) + Mi_1(t)i_2(t) + \frac{1}{2}L_2 i_2^2(t)$$

MUST COMPUTE $M, i_1(t), i_2(t)$

$$L_1, L_2, k \Rightarrow M = k \sqrt{L_1 L_2} \quad M = 5.31\text{mH}$$

$$\omega L_1 = 377 \times 2.653 \times 10^{-3} = 1\Omega$$

$$\omega L_2 = 4\Omega, \omega M = 2\Omega$$



Circuit in frequency domain

Assume steady state operation

We can use frequency domain techniques

Merge the writing of the loop and coupled inductor equations in one step

$$2I_1 + (j1I_1 - j2I_2) = 24\angle 0^\circ$$

$$4I_2 - (j2I_1 - j4I_2) = 0$$

SOLVE TO GET

$$I_1 = 9.41\angle -11.31^\circ(A), I_2 = 3.33\angle 33.69^\circ(A)$$

$$\therefore i_1(t) = 9.41 \cos(377t - 11.31^\circ)(A)$$

$$i_2(t) = 3.33 \cos(377t + 33.69^\circ)(A)$$

WARNING : The term $377t$ is in radians!

$$t = 0.005\text{s} \Rightarrow 377t = 1.885(\text{rad}) = 108^\circ$$

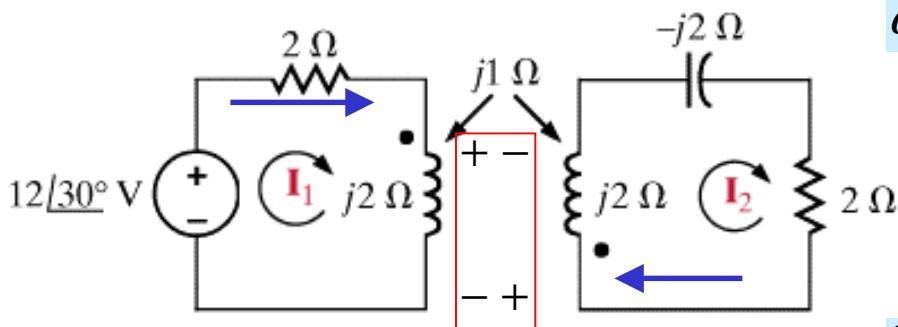
$$i_1(0.005) = -1.10(A), i_2(0.005) = -2.61(A)$$

$$w(0.005) = 0.5 \times 2.653 \times 10^{-3} (-1.10)^2 \\ + 5.31 \times 10^{-3} (-1.10) \times (-2.61) \\ + 0.5 \times 101.61 \times 10^{-3} \times (-2.61)^2 (J)$$

$$w(0.005) = 22.5\text{mJ}$$

LEARNING EXTENSION

$$f = 60 \text{ Hz}$$



$$w(t) = \frac{1}{2} L_1 i_1^2(t) - M i_1(t) i_2(t) + \frac{1}{2} L_2 i_2^2(t)$$

$$\begin{aligned} 2I_1 + (j2I_1 + j1I_2) &= 12\angle 30^\circ \\ (j1I_1 + j2I_2) + (2 - j2)I_2 &= 0 \\ (2 + j2)I_1 + jI_2 &= 12\angle 30^\circ \\ jI_1 + 2I_2 &= 0 \quad \Rightarrow I_2 = -0.5jI_1 \\ (2 + j2 + 0.5)I_1 &= 12\angle 30^\circ \end{aligned}$$

$$I_1 = \frac{12\angle 30^\circ}{2.5 + j2} = \frac{12\angle 30^\circ}{3.20\angle 38.66^\circ} = 3.75\angle -8.66^\circ(A)$$

$$\begin{aligned} I_2 &= -0.5jI_1 = 0.5\angle -90^\circ \times 3.75\angle -8.66^\circ \\ &= 1.875\angle -98.66^\circ \end{aligned}$$

DETERMINE ENERGY STORED AT $t = 10 \text{ ms}$

$$f = 60 \text{ Hz} \Rightarrow \omega = 378.9(s^{-1})$$

$$\begin{aligned} \omega L_1 &= 2 \Rightarrow L_1 = 0.00528(H) = L_2 \\ M &= 0.00264(H) \end{aligned}$$

$$i_1(t) = 3.75 \cos(378.9t - 8.66^\circ)(A)$$

$$i_2(t) = 1.875 \cos(378.9t - 98.66^\circ)(A)$$

$$378.9(\text{rad/sec}) \times 0.010(\text{sec}) = 3.789(\text{rad}) = 217.1^\circ$$

$$i_1(0.010) = -3.3(A)$$

$$i_2(0.010) = -0.91(A)$$

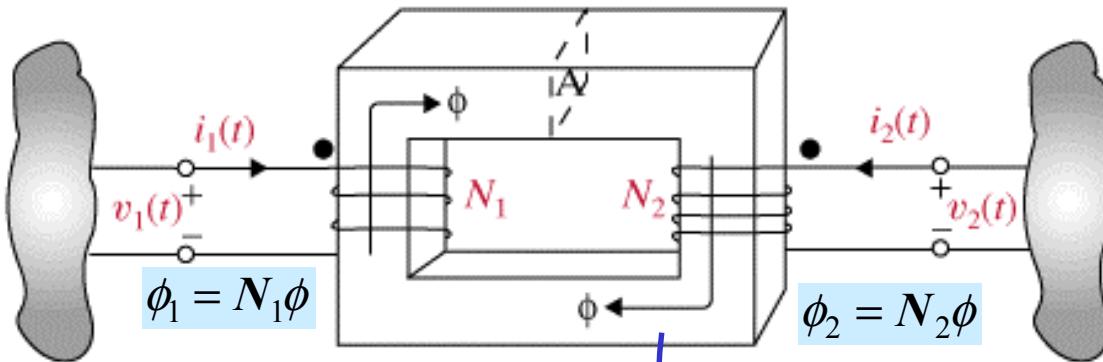
$$\begin{aligned} w(0.010) &= 0.5 * 0.00528 * (-3.3)^2 \\ &\quad - 0.00264 * (-3.3)(-0.91) \\ &\quad + 0.5 * 0.00528 * (0.91)^2(J) \end{aligned}$$

$$w(0.010) = 0.00264 * (3.3^2 - (3.3)(0.91) + 0.91^2)$$

$$w(0.010) = 0.030J = 30mJ$$

Go back to time domain

THE IDEAL TRANSFORMER



$$\left. \begin{aligned} v_1(t) &= N_1 \frac{d\phi}{dt}(t) \\ v_2(t) &= N_2 \frac{d\phi}{dt}(t) \end{aligned} \right\} \Rightarrow \frac{v_1}{v_2} = \frac{N_1}{N_2}$$

First ideal transformer equation

$$v_1(t)i_1(t) + v_2(t)i_2(t) = 0$$

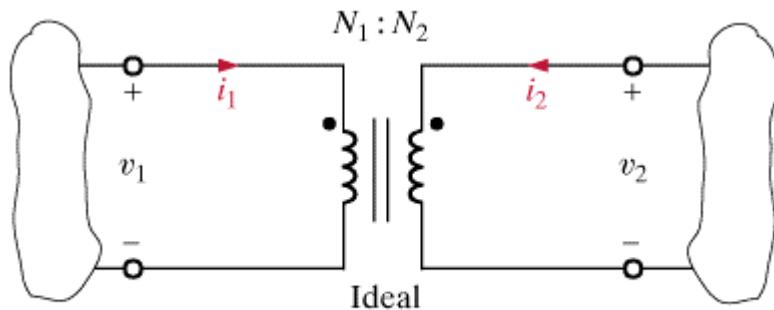
Ideal transformer is lossless

$$\frac{i_1}{i_2} = -\frac{N_2}{N_1}$$

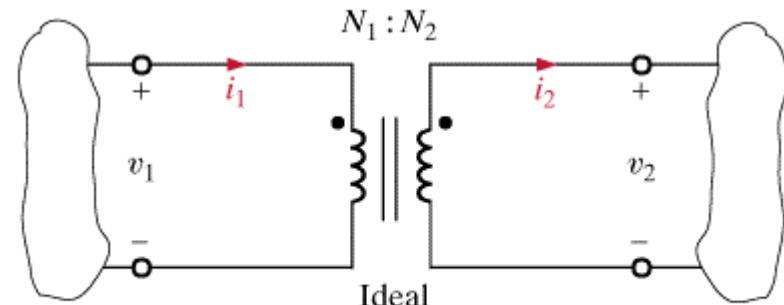
Second ideal transformer equations

Insures that 'no magnetic flux goes astray'

Since the equations are algebraic, they are unchanged for Phasors. Just be careful with signs



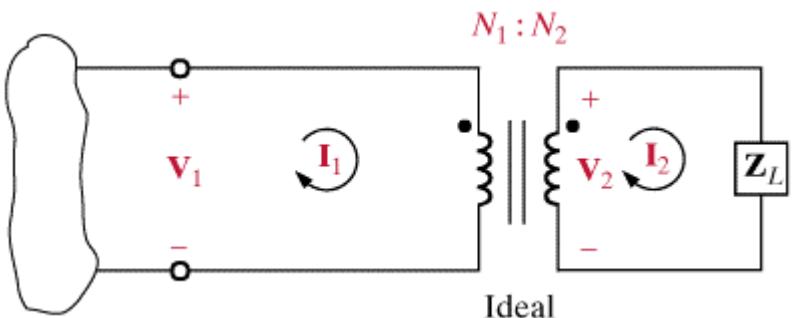
Circuit Representations



$$\frac{v_1}{v_2} = \frac{N_1}{N_2}; \quad \frac{i_1}{i_2} = -\frac{N_2}{N_1}$$



REFLECTING IMPEDANCES



$$\frac{V_1}{V_2} = \frac{N_1}{N_2} \text{ (both + signs at dots)}$$

$$\frac{I_1}{I_2} = \frac{N_2}{N_1} \text{ (Current } I_2 \text{ leaving transformer)}$$

$$V_2 = Z_L I_2 \text{ (Ohm's Law)}$$

$$V_1 \frac{N_2}{N_1} = Z_L I_1 \frac{N_1}{N_2}$$

$$V_1 = \left(\frac{N_1}{N_2} \right)^2 Z_L I_1$$

$$\frac{V_1}{I_1} = Z_1 = \left(\frac{N_1}{N_2} \right)^2 Z_L$$

Z_1 = impedance, Z_L , reflected
into the primary side

For future reference

$$S_1 = V_1 I_1^* = \left(V_2 \frac{N_1}{N_2} \right) \left(I_2 \frac{N_2}{N_1} \right)^* = V_2 I_2^* = S_2$$

$$n = \frac{N_2}{N_1} = \text{turns ratio}$$

Phasor equations for ideal transformer

$$V_1 = \frac{V_2}{n}$$

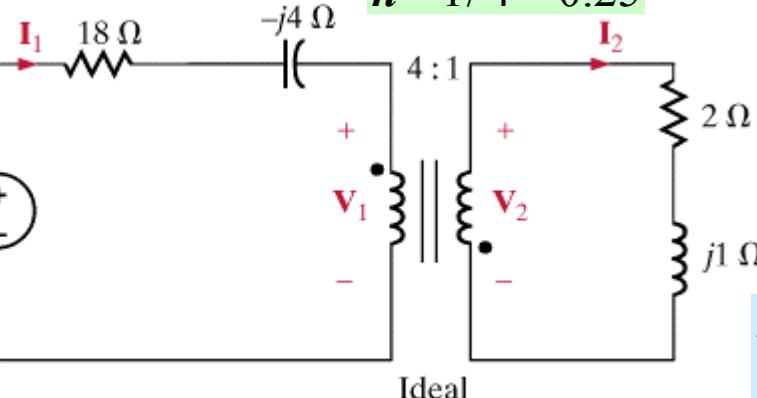
$$I_1 = n I_2$$

$$Z_1 = \frac{Z_L}{n^2}$$

$$S_1 = S_2$$

LEARNING EXAMPLE

Determine all indicated voltages and currents



$$I_1 = \frac{120\angle 0^\circ}{50 + j12} = \frac{120\angle 0^\circ}{51.42\angle 13.5^\circ} = 2.33\angle -13.5^\circ$$

$$V_1 = Z_1 I_1 = \frac{Z_1}{Z_1 + Z_2} 120\angle 0^\circ$$

$$Z_1 I_1 = (32 + j16) \times 2.33\angle -13.5^\circ$$

SAME COMPLEXITY

$$\frac{Z_1}{Z_1 + Z_2} 120\angle 0^\circ = \frac{32 + j16}{51.42\angle 13.5^\circ} \times 120$$

$$V_1 = 35.78\angle 26.57^\circ \times 2.33\angle -13.5^\circ = 83.36\angle 13.07^\circ$$

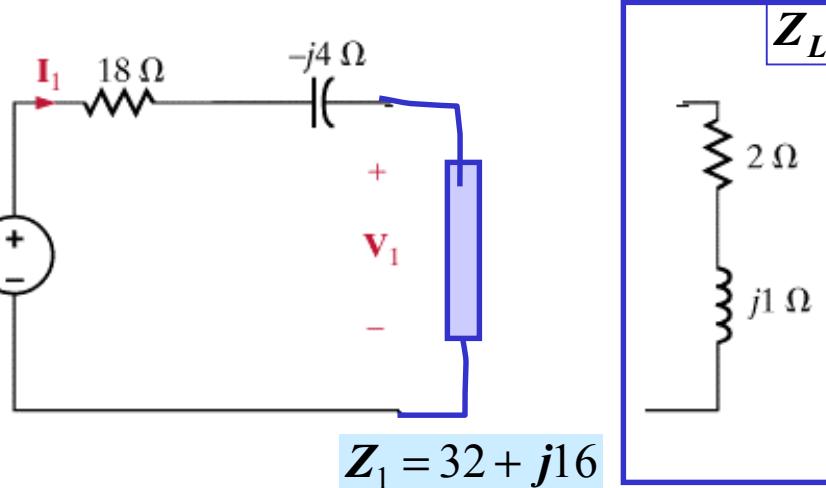
Strategy: reflect impedance into the primary side and make transformer "transparent to user."

$$Z_1 = \frac{Z_L}{n^2}$$

CAREFUL WITH POLARITIES AND CURRENT DIRECTIONS!

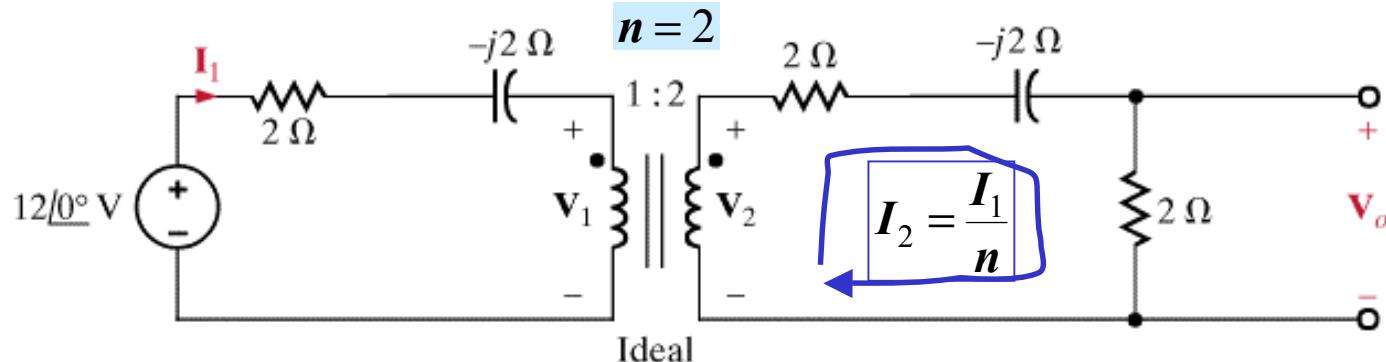
$$I_2 = \frac{I_1}{n} = -4I_1 \text{ (current into dot)}$$

$$V_2 = -nV_1 = -0.25V_1 \text{ (+ is opposite to dot)}$$



LEARNING EXTENSION

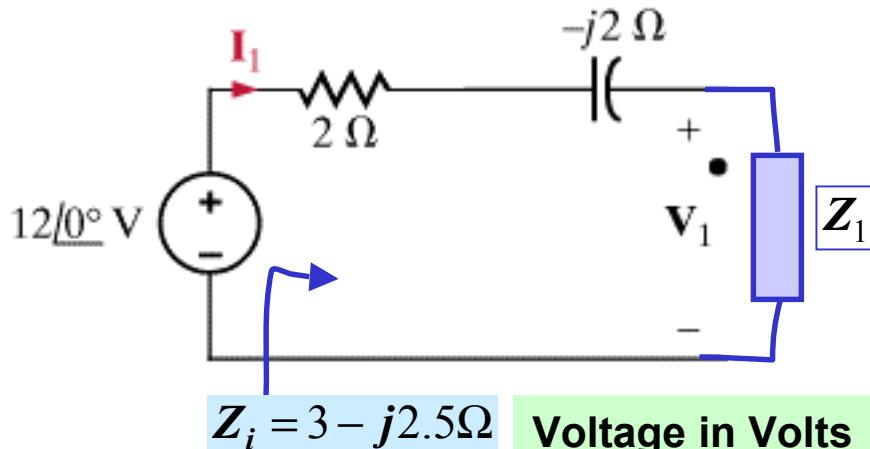
Find the current I_1



Strategy: reflect impedance into the primary side and make transformer "transparent to user."

$$Z_1 = \frac{Z_L}{n^2}$$

$$Z_1 = \frac{4 - j2}{4} = 1 - j0.5 \Omega$$



Voltage in Volts
Impedance in Ohms
...Current in Amps

$$I_1 = \frac{12\angle 0^\circ}{3 - j2.5} = \frac{12\angle 0^\circ}{3.91\angle -39.81^\circ} = 3.07\angle 39.81^\circ (\text{A})$$

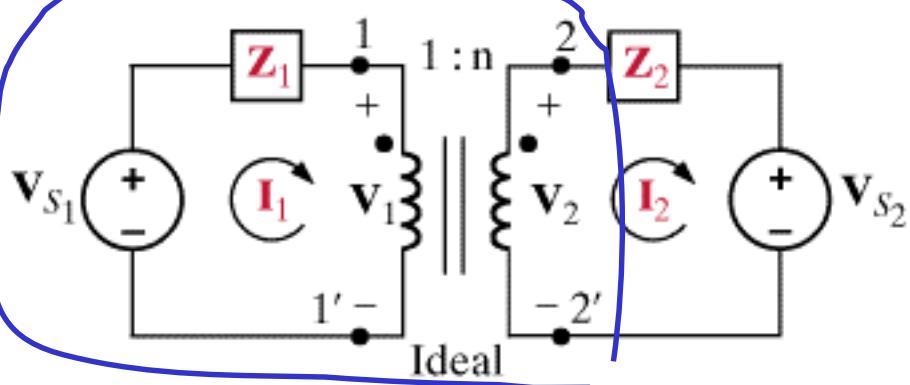
LEARNING EXTENSION

Find V_o

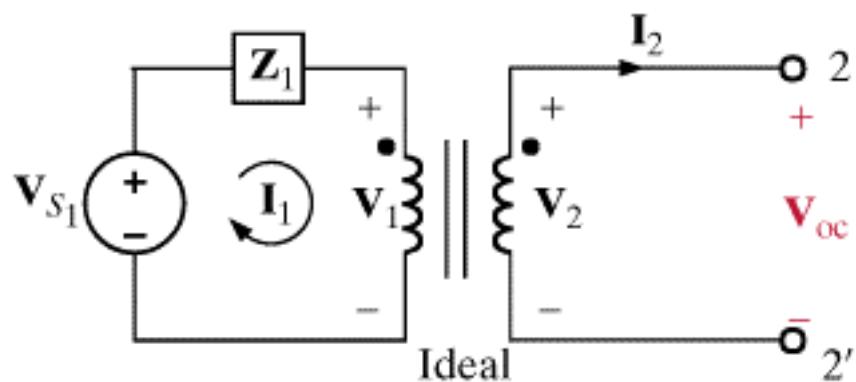
Strategy: Find current in secondary and then use Ohm's Law

$$I_2 = \frac{I_1}{2} \Rightarrow V_o = 2\Omega \times \frac{I_1}{2} = 3.07\angle 39.81^\circ (\text{V})$$

USING THEVENIN'S THEOREM TO SIMPLIFY CIRCUITS WITH IDEAL TRANSFORMERS



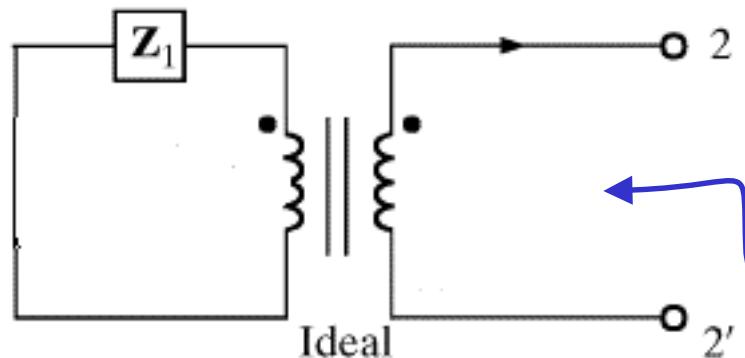
Replace this circuit with its Thevenin equivalent



$$\left. \begin{array}{l} I_2 = 0 \\ I_1 = nI_2 \end{array} \right\} \Rightarrow I_1 = 0 \Rightarrow V_1 = V_{S1}$$

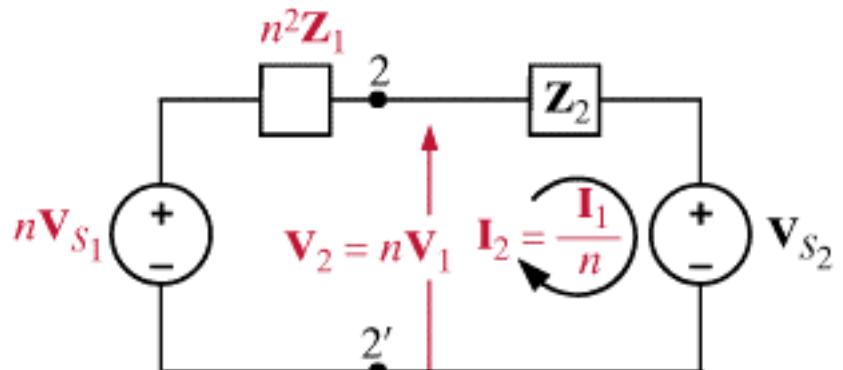
$$\left. \begin{array}{l} V_1 = V_{S1} \\ V_2 = nV_1 \end{array} \right\} \Rightarrow V_{oc} = nV_{S1}$$

To determine the Thevenin impedance...



Reflect impedance into secondary

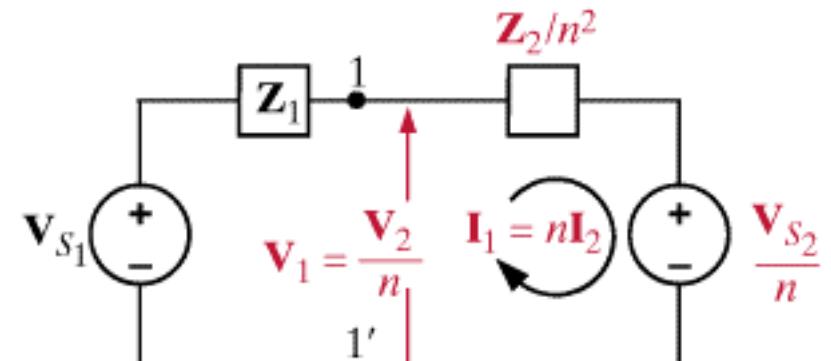
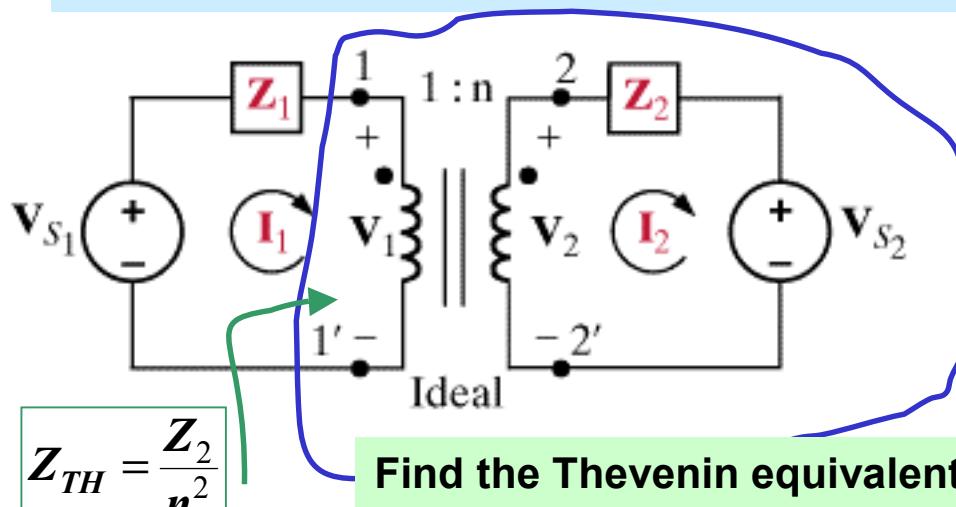
$$Z_{TH} = n^2 Z_1$$



Equivalent circuit with transformer "made transparent."

One can also determine the Thevenin equivalent at 1 - 1'

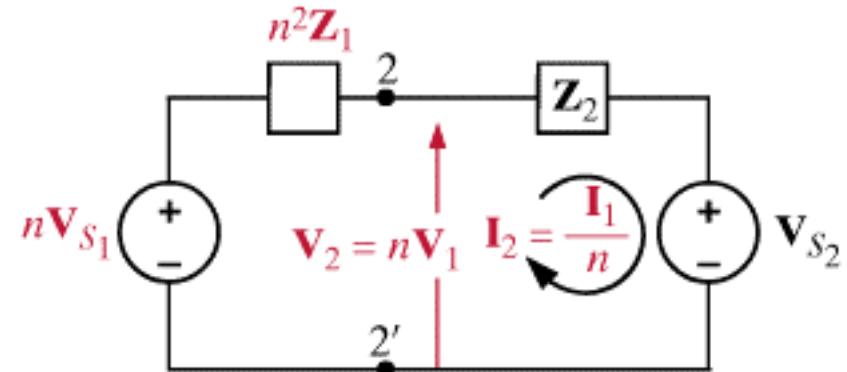
USING THEVENIN'S THEOREM: REFLECTING INTO THE PRIMARY



In open circuit $I_1 = 0$ and $I_2 = 0$

$$V_{OC} = \frac{V_{S2}}{n}$$

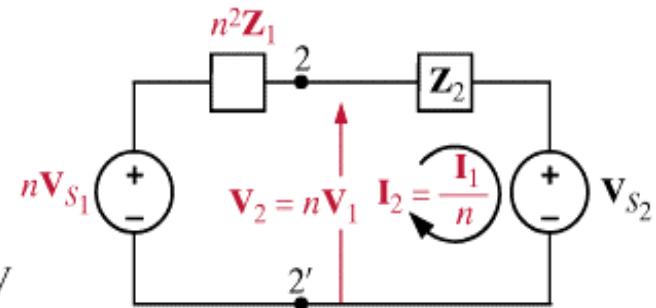
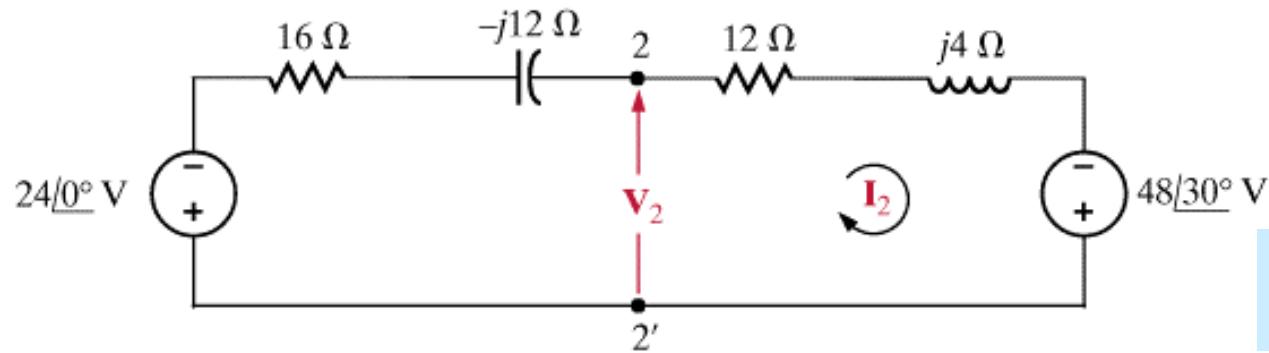
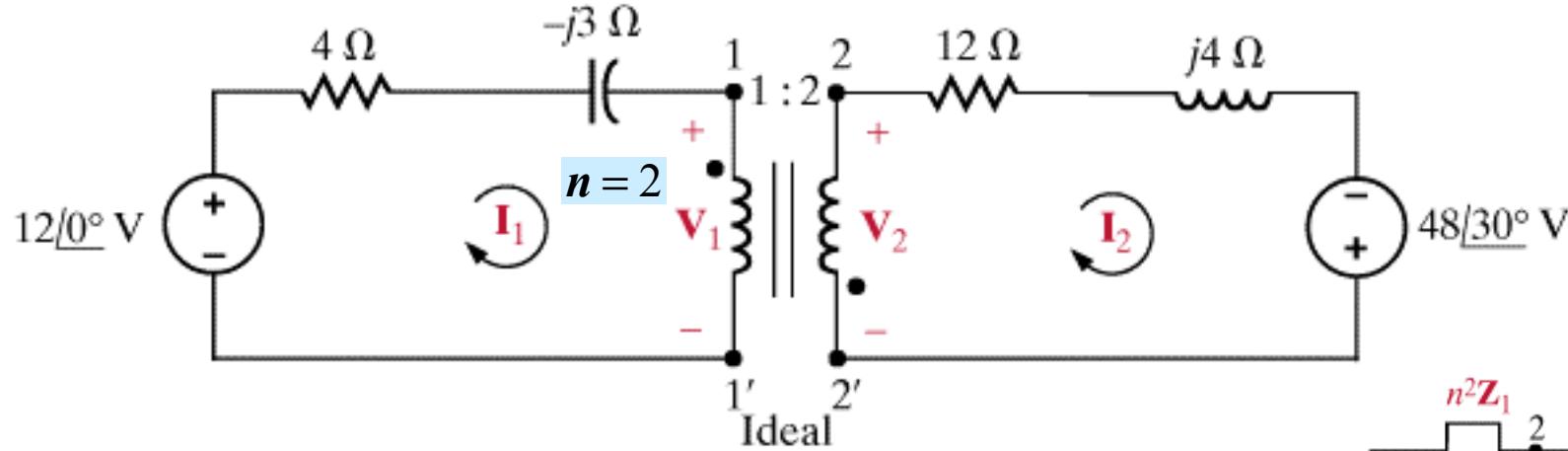
Thevenin impedance will be the secondary impedance reflected into the primary circuit



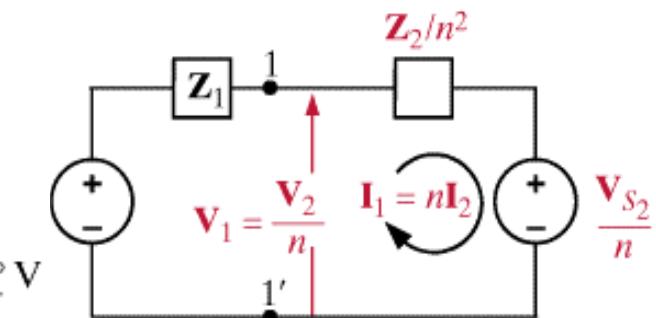
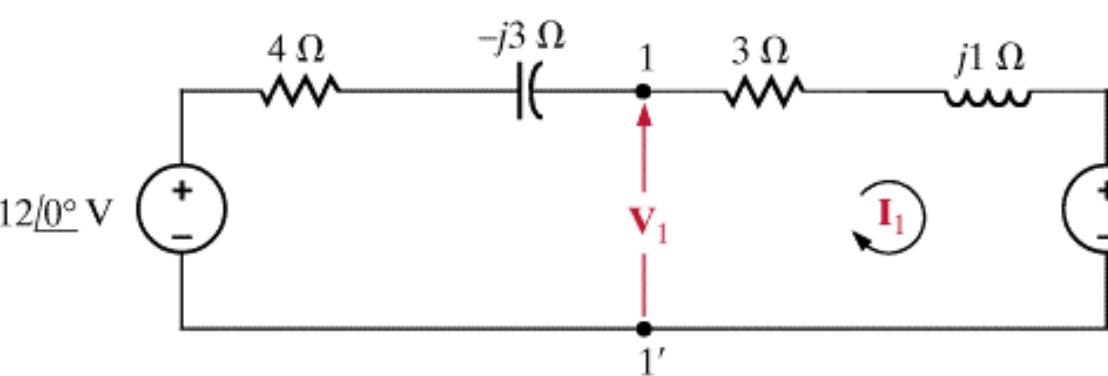
Equivalent circuit reflecting into secondary

LEARNING EXAMPLE

Draw the two equivalent circuits



Equivalent circuit reflecting into secondary

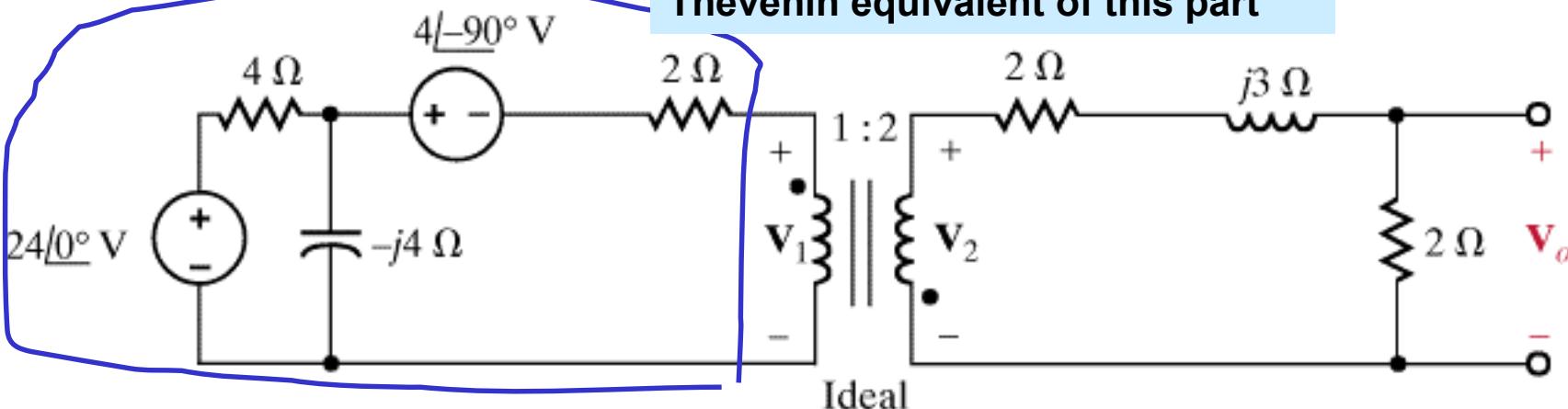


Equivalent circuit reflecting into primary

LEARNING EXAMPLE

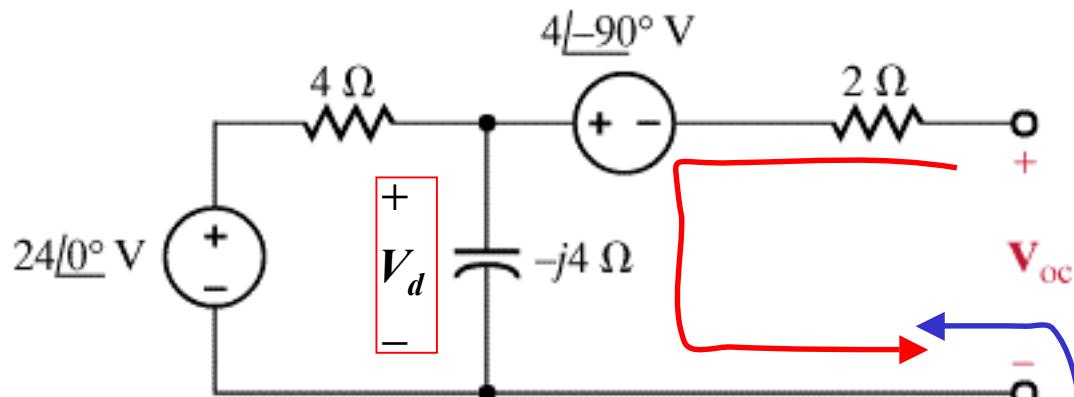
Find V_o

Thevenin equivalent of this part



To compute V_o is better to reflect into secondary

But before doing that it is better to simplify the primary using Thevenin's Theorem



$$Z_{TH} = 2 + \frac{-j16}{4-j4} = \frac{8-j8-j16}{4-j4}$$

$$Z_{TH} = \frac{2-j6}{1-j} \times \frac{1+j}{1+j} = \frac{8-j4}{2}$$

$$V_{OC} = V_d - 4\angle -90^\circ$$

$$V_d = \frac{-j4}{4-j4} 24\angle 0^\circ = \frac{24\angle -90^\circ}{1-j}$$

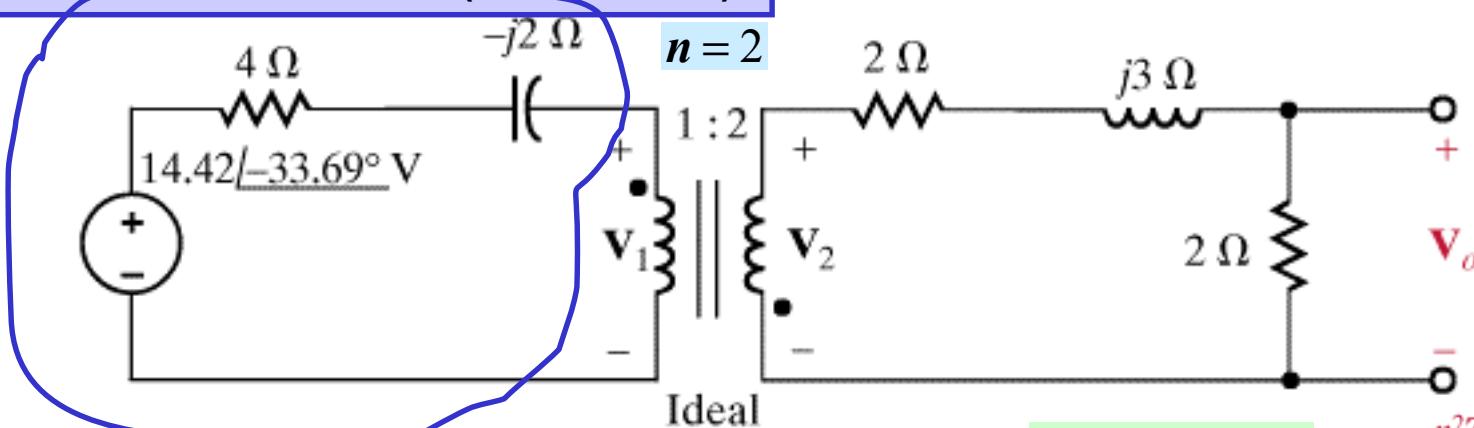
$$V_{OC} = 14.47\angle -33.69^\circ (V)$$

$$Z_{TH} = 2 + (4 \parallel -j4) \quad Z_{TH} = 4 - j2(\Omega)$$

This equivalent circuit is now transferred to the secondary

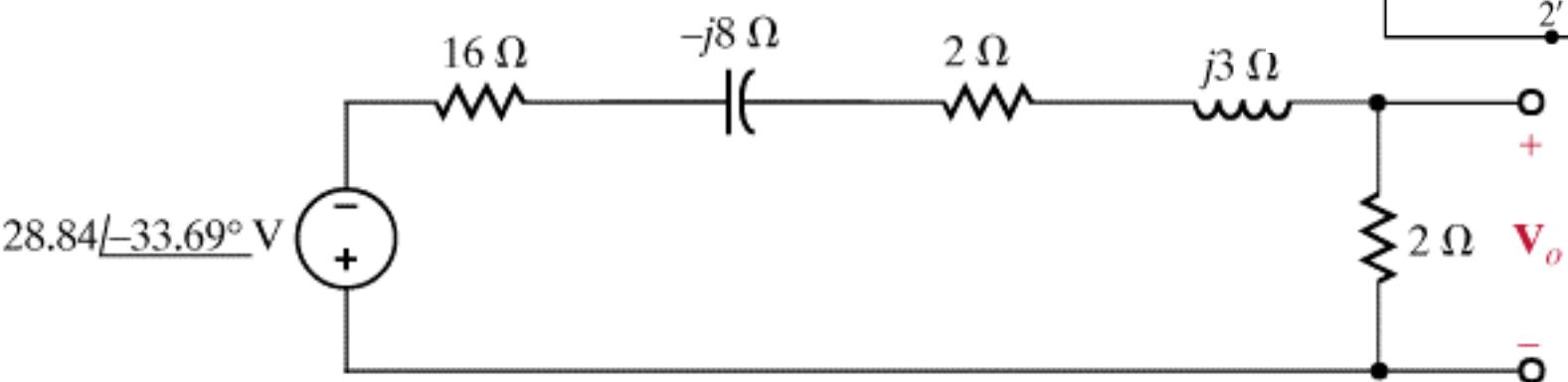
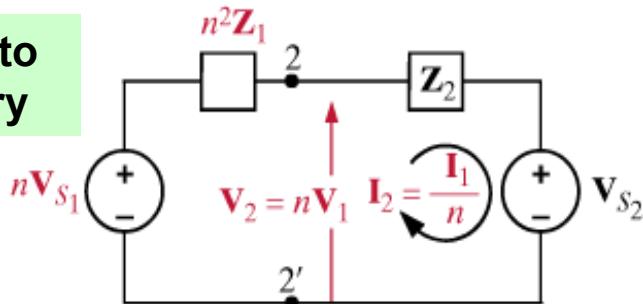


LEARNING EXAMPLE (continued...)



Thevenin equivalent of primary side

Transfer to secondary

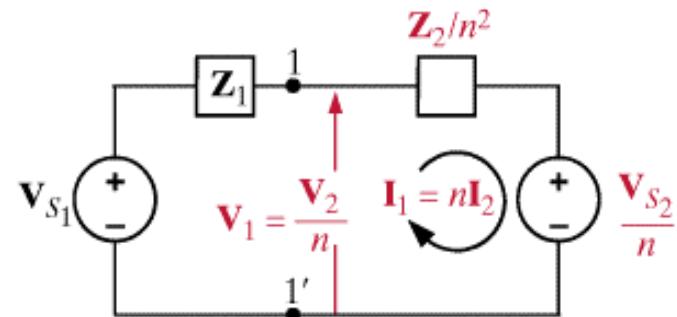
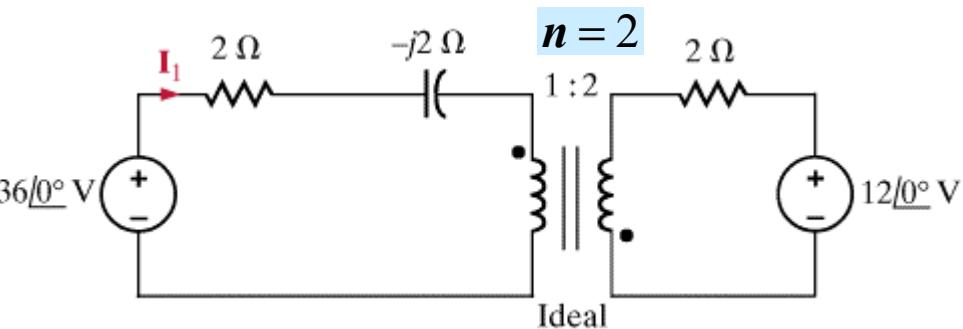


Circuit with primary transferred to secondary

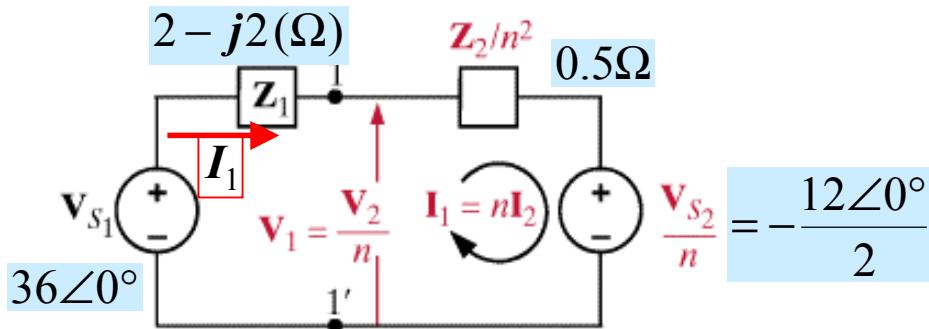
$$V_o = \frac{2}{20 - j5} 28.84 \angle -33.69^\circ = \frac{2 \times 28.84 \angle -33.69^\circ}{20.62 \angle -14.04^\circ}$$

LEARNING EXTENSION

Find I_1



Equivalent circuit reflecting
into primary



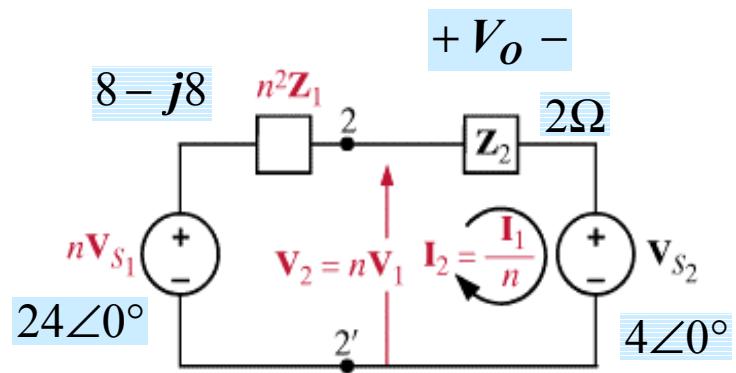
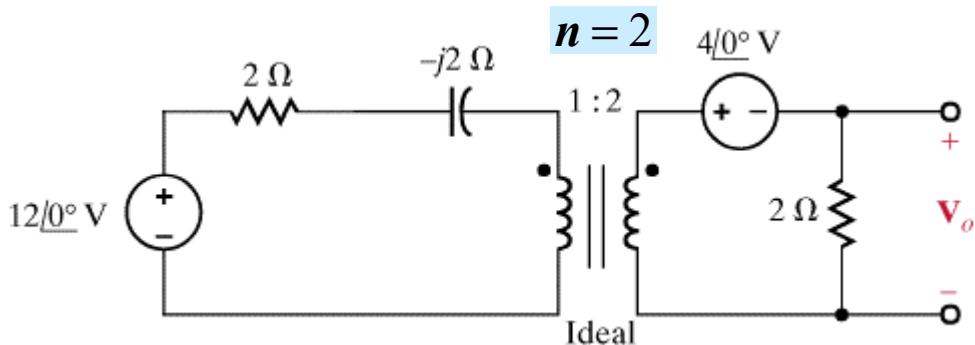
Notice the position of the
dot marks

$$I_1 = \frac{36\angle 0^\circ + 6\angle 0^\circ}{2 - j1.5}$$

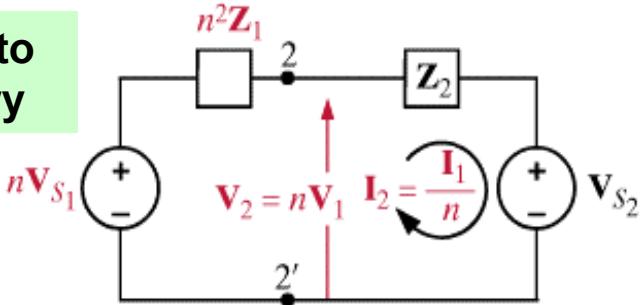
$$I_1 = \frac{36\angle 0^\circ}{2.5\angle -36.86^\circ}$$

LEARNING EXTENSION

Find V_o



Transfer to
secondary

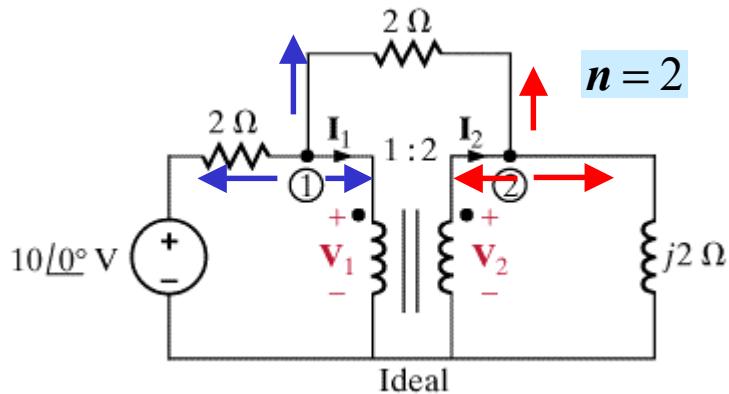


$$V_o = \frac{2}{(8 - j8) + 2} 20\angle 0^\circ$$

$$V_o = \frac{40\angle 0^\circ}{12.81\angle -38.66^\circ}$$

LEARNING EXAMPLE

Find I_1, I_2, V_1, V_2



Nothing can be transferred. Use transformer equations and circuit analysis tools

Phasor equations for ideal transformer

$$V_1 = \frac{V_2}{n}$$

$$I_1 = nI_2$$

@ Node 1: $\frac{V_1 - 10\angle 0^\circ}{2} + \frac{V_1 - V_2}{2} + I_1 = 0$

@Node 2: $\frac{V_2 - V_1}{2} + \frac{V_2}{j2} - I_2 = 0$

4 equations in 4 unknowns!

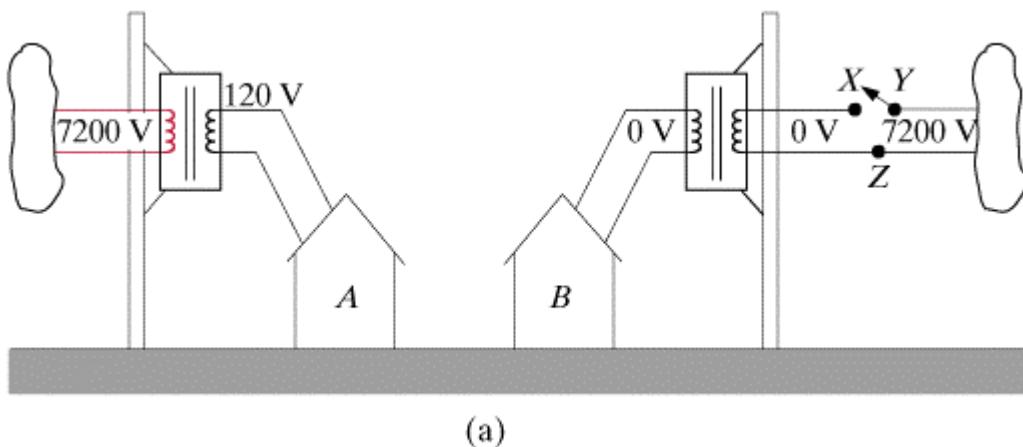
$$\begin{aligned} 2V_1 - V_2 + 2I_1 &= 10\angle 0^\circ \Rightarrow I_1 = 5\angle 0^\circ \\ -V_1 + (1-j)V_2 - 2I_2 &= 0 \\ V_2 &= 2V_1 \\ I_1 &= 2I_2 \quad \longrightarrow I_2 = 2.5\angle 0^\circ \\ -V_1 + (1-j)(2V_1) &= 5\angle 0^\circ \end{aligned}$$

$$V_1 = \frac{5\angle 0^\circ}{1-j2} = \frac{5\angle 0^\circ}{2.24\angle -63.43^\circ} = \sqrt{5}\angle 63.43^\circ$$

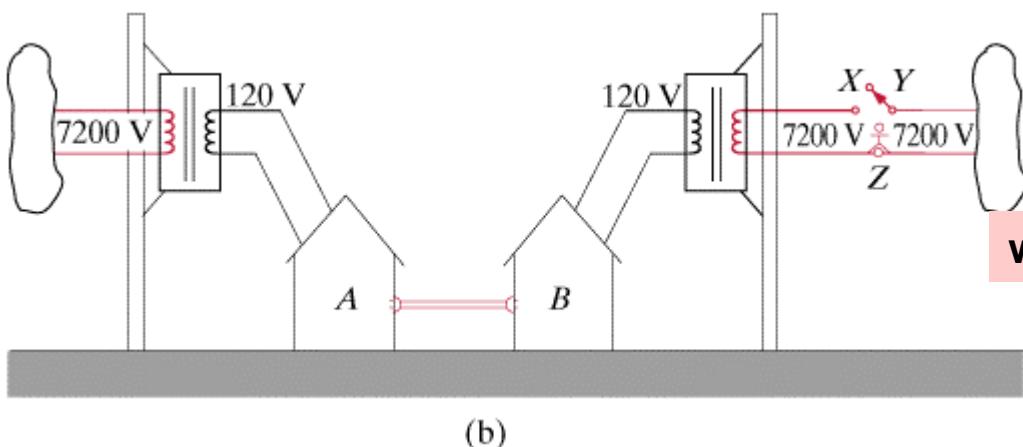
$$V_2 = 2\sqrt{5}\angle 63.43^\circ$$

SAFETY CONSIDERATIONS: AN EXAMPLE

Houses fed from different distribution transformers



Braker X-Y opens, house B is powered down



When technician resets the
braker he finds 7200V between
points X-Z

when he did not expect to find any

Good neighbor runs an extension
and powers house B

CASE STUDY: Transmit 24MW over 100miles with 95% efficiency

A. AT 240V
B. AT 240kV

Given: Conductor resistance, $R = \frac{\rho l}{A}$

ρ = resistivity of material (e.g., copper = $8 \times 10^{-8} \Omega/m$)

l = length of conductor = $160.9 \text{ Km} = 1.609 \times 10^5 \text{ m}$

A = cross section = πr^2

Required: Maximum losses, $P_{loss} = 24 \text{ MW} \times 0.05 = 1.2 \text{ MW}$

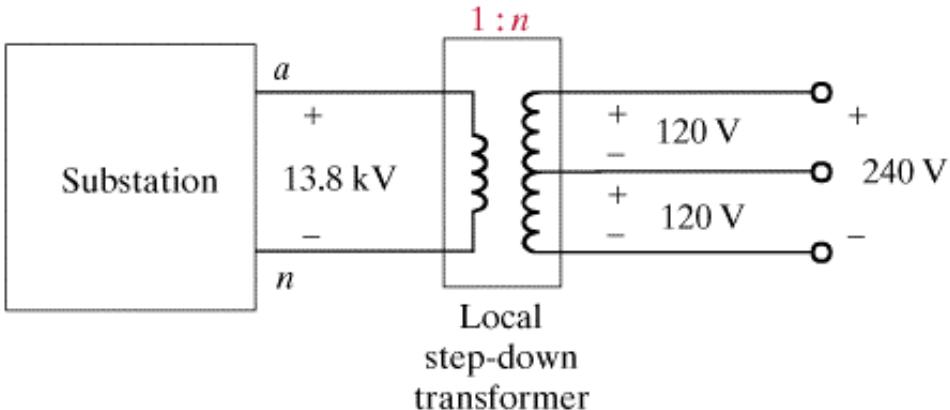
Known: Line losses : $P_{loss} = RI^2$

A. At 240V one needs a current $I_l = \frac{24 \times 10^6 W}{240 V} = 10^5 A$

$$1.2 \times 10^6 W = 2 \times \frac{8 \times 10^{-8} \times 1.609 \times 10^5}{\pi r^2} \times 10^{10} \Rightarrow r = 8.624 m$$

B. At 240kV one needs a current $I_l = \frac{24 \times 10^6 W}{240 \times 10^3 V} = 10^2 A$

$$1.2 \times 10^6 W = 2 \times \frac{8 \times 10^{-8} \times 1.609 \times 10^5}{\pi r^2} \times 10^4 \Rightarrow r = 0.8624 cm$$



Households per transformer = 10
Maximum current per household = 200A

Determining ratio

$$\frac{V_2}{V_1} = n \Rightarrow n = \frac{240}{13800} = \frac{1}{57.5}$$

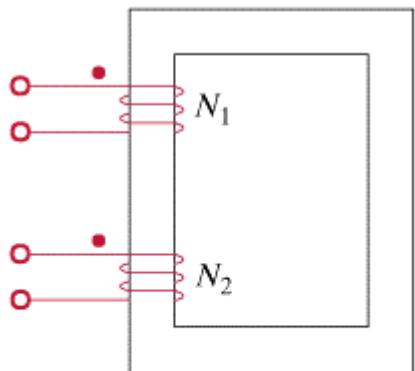
Determining power rating

Max secondary current = 2000A

$$n = \frac{I_1}{I_2} \Rightarrow I_1 = \frac{2000}{57.6} = 34.78A$$

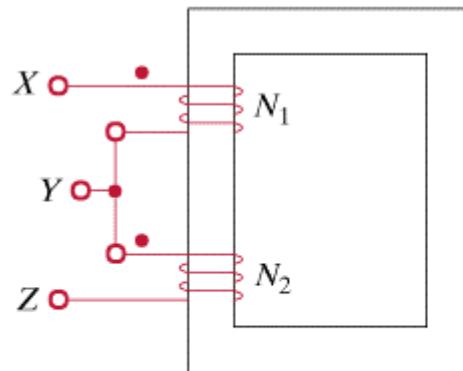
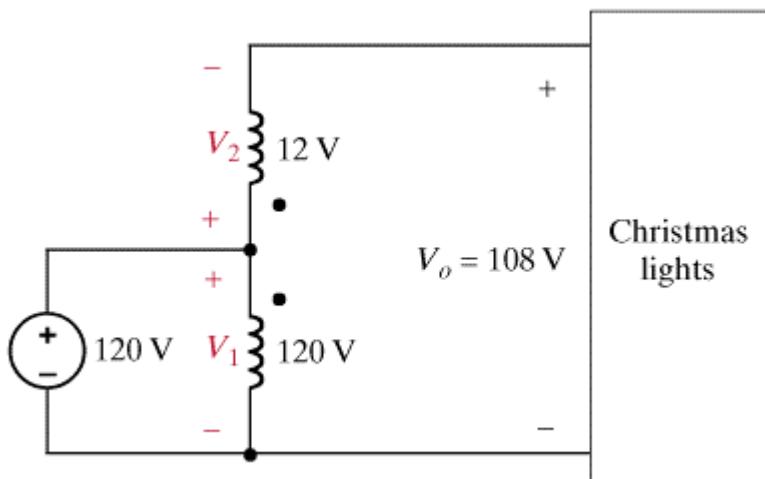
$$\therefore P = 13,800 \times 34.78 = 480kVA$$

Also : $P = 240(V) \times 2000(A)$

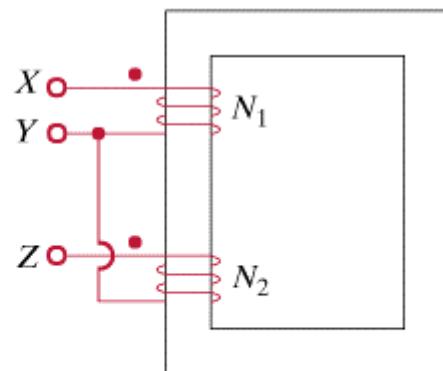


Conventional transformer

Use the subtractive connection on the 120V - 12V transformer



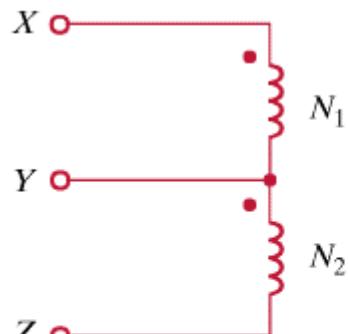
Additive connection



Subtractive connection

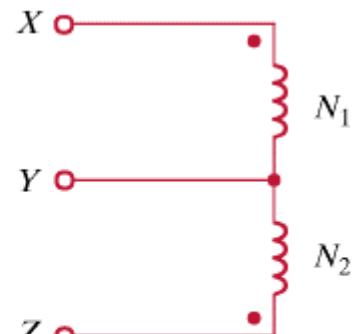
Auto transformer connections

$$V_{xz} = V_{xy} + V_{yz}$$



Additive connection

$$V_{xz} = V_{xy} - V_{yz}$$



Subtractive connection

Circuit representations

Transformers

